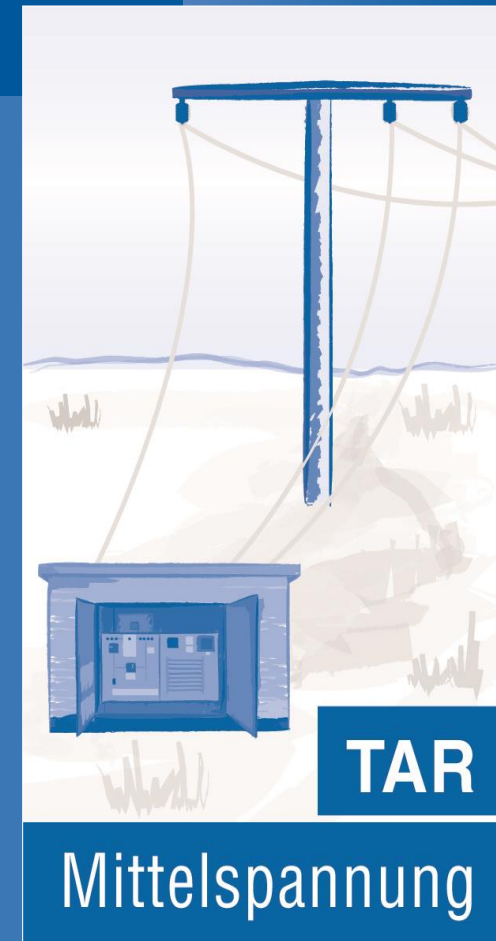


# Summary of the draft VDE-AR-N 4110:2017-02

The following summary:

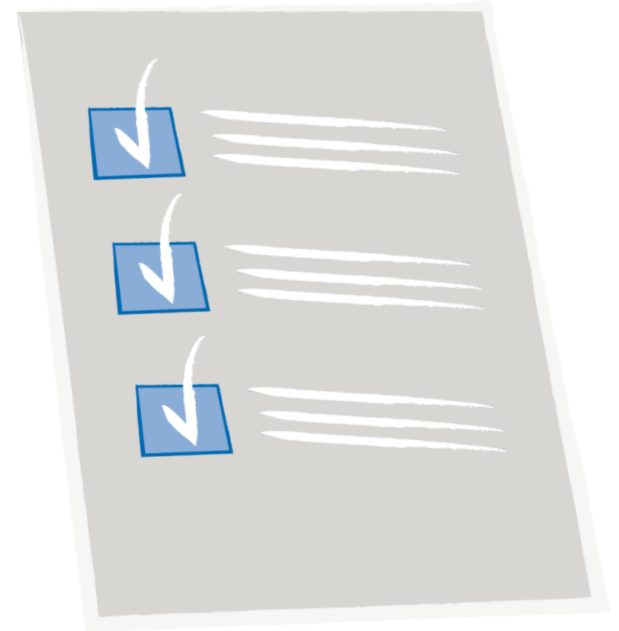
- does not cover all parts of the VDE-AR-N 4110 and is therefore not exhaustive;
- mainly covers the technical requirements for customer installations;
- and is purely informative.

February 2017



## Overview

- Section 5 und 10.2.2 Static Voltage Stability
- Section 10.2.3 Dynamic Grid Support
- Section 10.2.4 Active Power Supply
- Section 10.3 Protection systems and protection settings



Section 5 and 10.2.2

## Static Voltage Stability

## 10 power generating modules - Overview

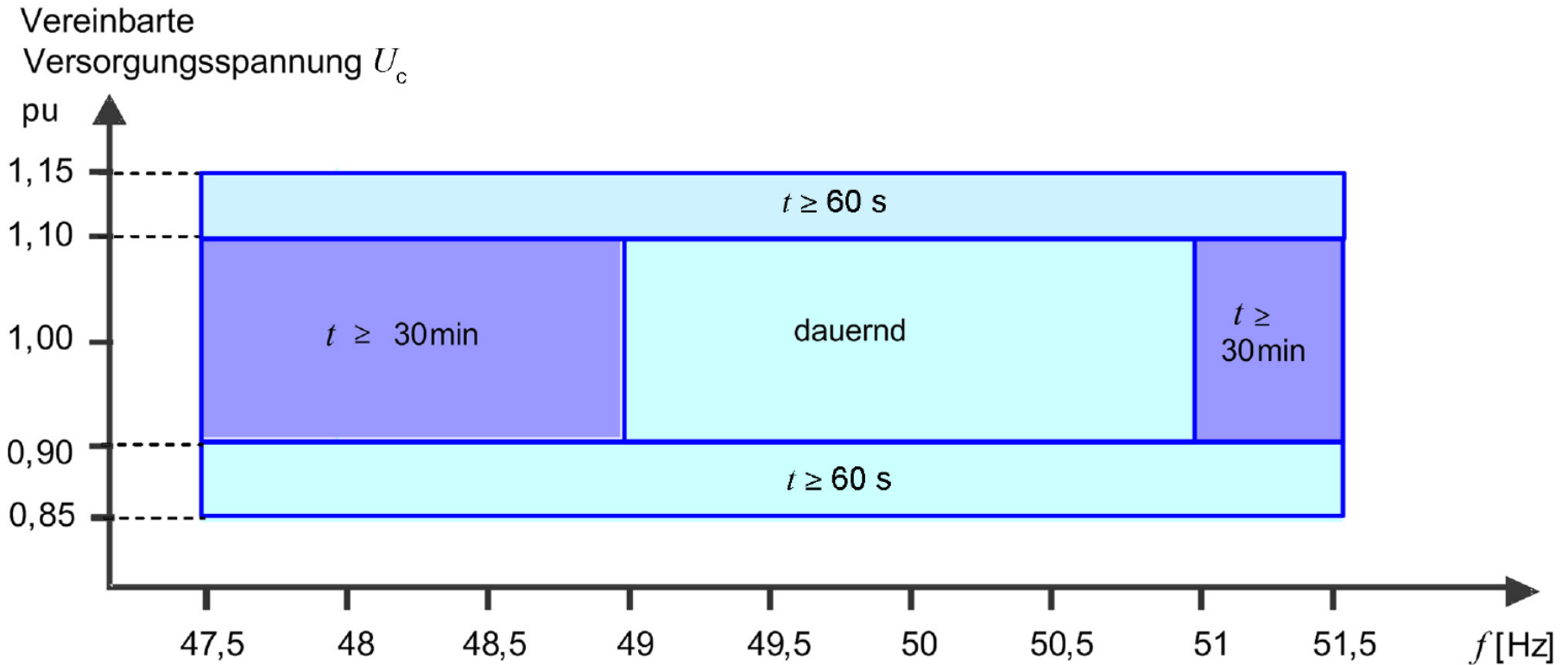
### Requirements for

- power generating modules and power generating units
- combined facilities of generation/demand/storage
- Storage

For combined facilities of generation/demand/storage it is important to note the

- Protection concept (10.3)
- Use of emergency generators (8.9)
- Frequency-dependent active power response (10.2.4.3)
- Dynamic grid support (10.2.3)
- Active power demand by the grid operator (reduction) (10.2.4.2)
- Static voltage stability (10.2.2)
- Evidence of electrical properties (11)

## 10.2 Behavior of the power generating module connected to the grid during steady-state operation



**Bild 4 – Anforderungen an den quasistationären Betrieb von Erzeugungsanlagen**

## 10.2 Behavior of the power generating module connected to the grid during steady-state operation

### Definition of steady-state operation

- Voltage gradient  $< 5 \% \ U_c \text{ min}^{-1}$
- Frequency gradient  $< 0.5 \% \ f_n \text{ min}^{-1}$

power generating modules must remain on the grid in steady-state operation, as per Figure 4

## 10.2 Behavior of the power generating module connected to the grid during steady-state operation

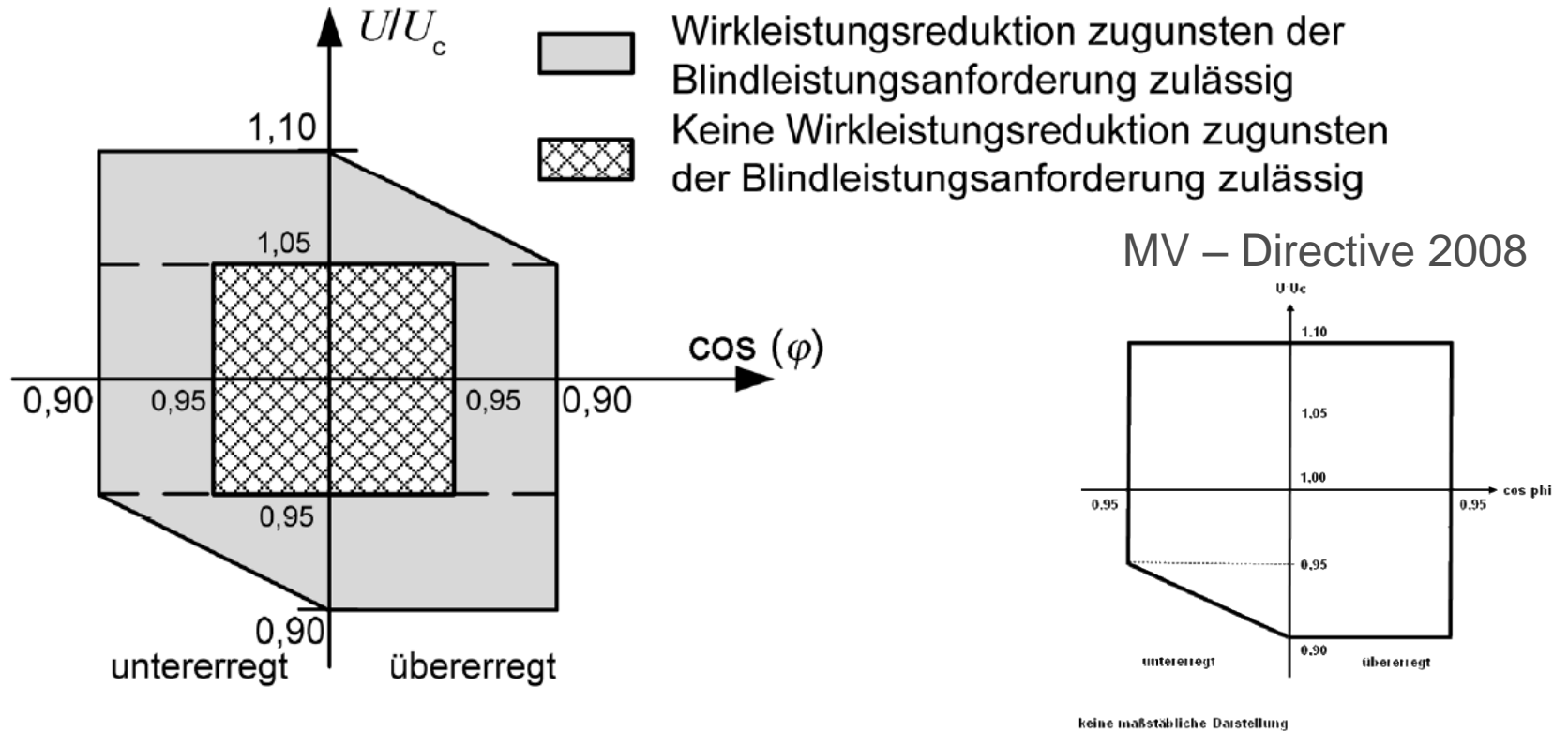
- In the voltage range from 90 %  $U_c$  to 110 %  $U_c$  voltage gradients of greater than  $5\% U_c \text{ min}^{-1}$  can occur.
- For voltages outside the voltage range 90 %  $U_c$  to 110 %  $U_c$  the active power and the reactive power supply can be reduced to protect the power generating module.

## 10.2 Behavior of the power generating module connected to the grid: Rotating or grid oscillation, subnetwork operability and Black Start capability

- Oscillations in the continental European grid with frequencies of 0.15 – 1.5 Hz
  - With this, the voltage can lie outside Figure 4 for a few seconds
  - For this reason, do not isolate supply from power generating modules when there is a symmetrical voltage curve in operation at  $0.8 U_c - 1.2 U_c$  for 5 sec.
  - During grid oscillation, the active power can be reduced to avoid overloading
- If a loss of stability occurs, the generation units must be isolated from the grid
- Subnetwork operability, Black Start capability, Isolated network and Black Start capability are not minimum requirements



## 10.2.2 Static voltage stability/ reactive power supply



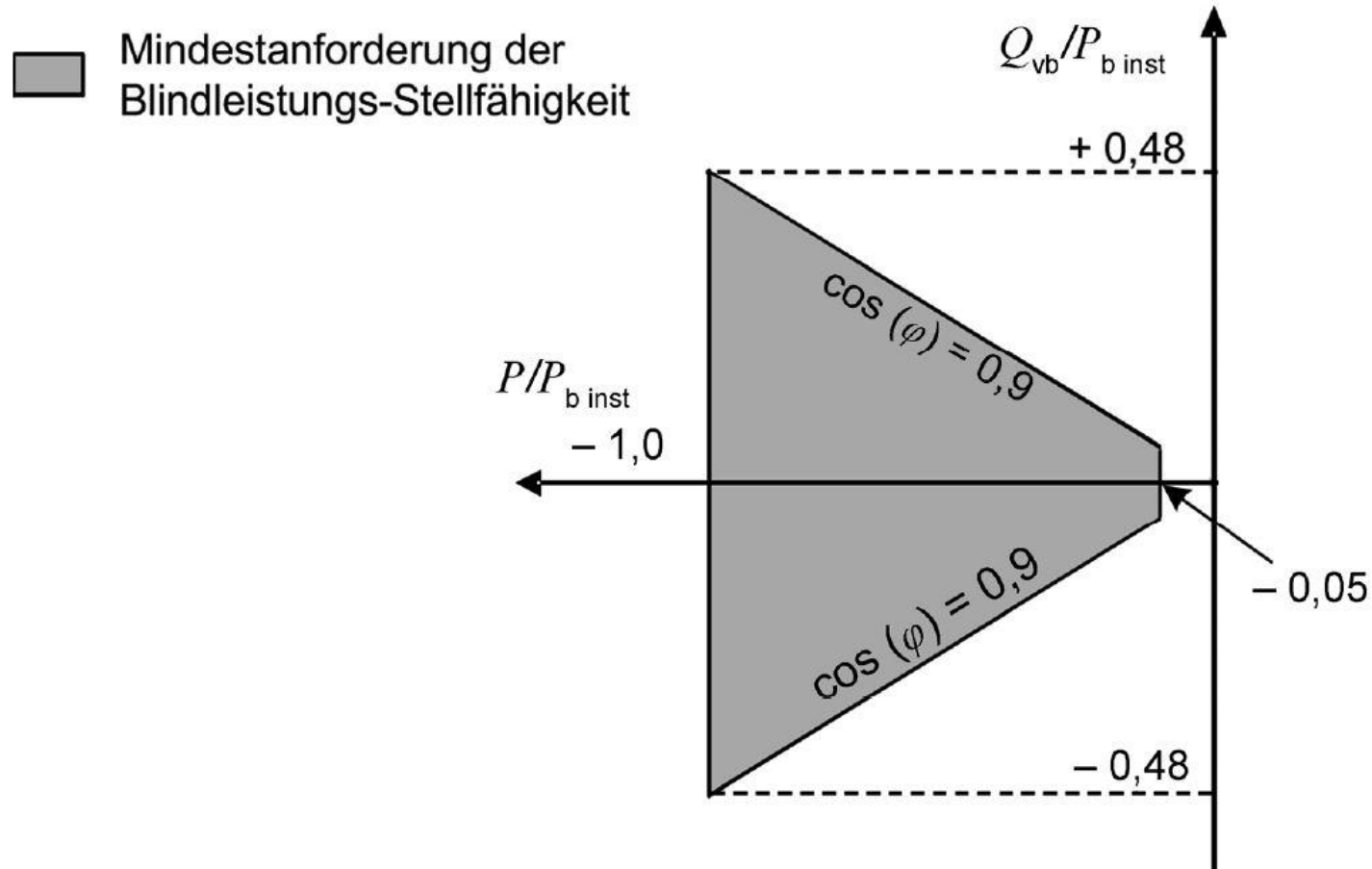
**Bild 5 – Anforderungen an Erzeugungsanlagen an die Blindleistungsbereitstellung am Netzanschlusspunkt**

## 10.2.2 Static voltage stability/ idle power supply

- Supply of reactive power in the power generating module to maintain voltage when slow (steady-state) voltage changes
- Requirements for the grid connection point
- Active power reduction of max. 10 %  $P_{b\ inst}$  permitted outside the shaded area in Figure 5

Note: The reactive power area in the design is not yet fully complete in the project group (see introduction)

## 10.2.2 Static voltage stability/ reactive power capability below $P_{b\ inst}$



**Bild 6 –  $P/Q$ -Diagramm der Erzeugungsanlage am Netzanschlusspunkt im Verbraucherzählpfeilsystem**

## 10.2.2 Static voltage stability/ reactive power supply less than $P_{b\ inst}$

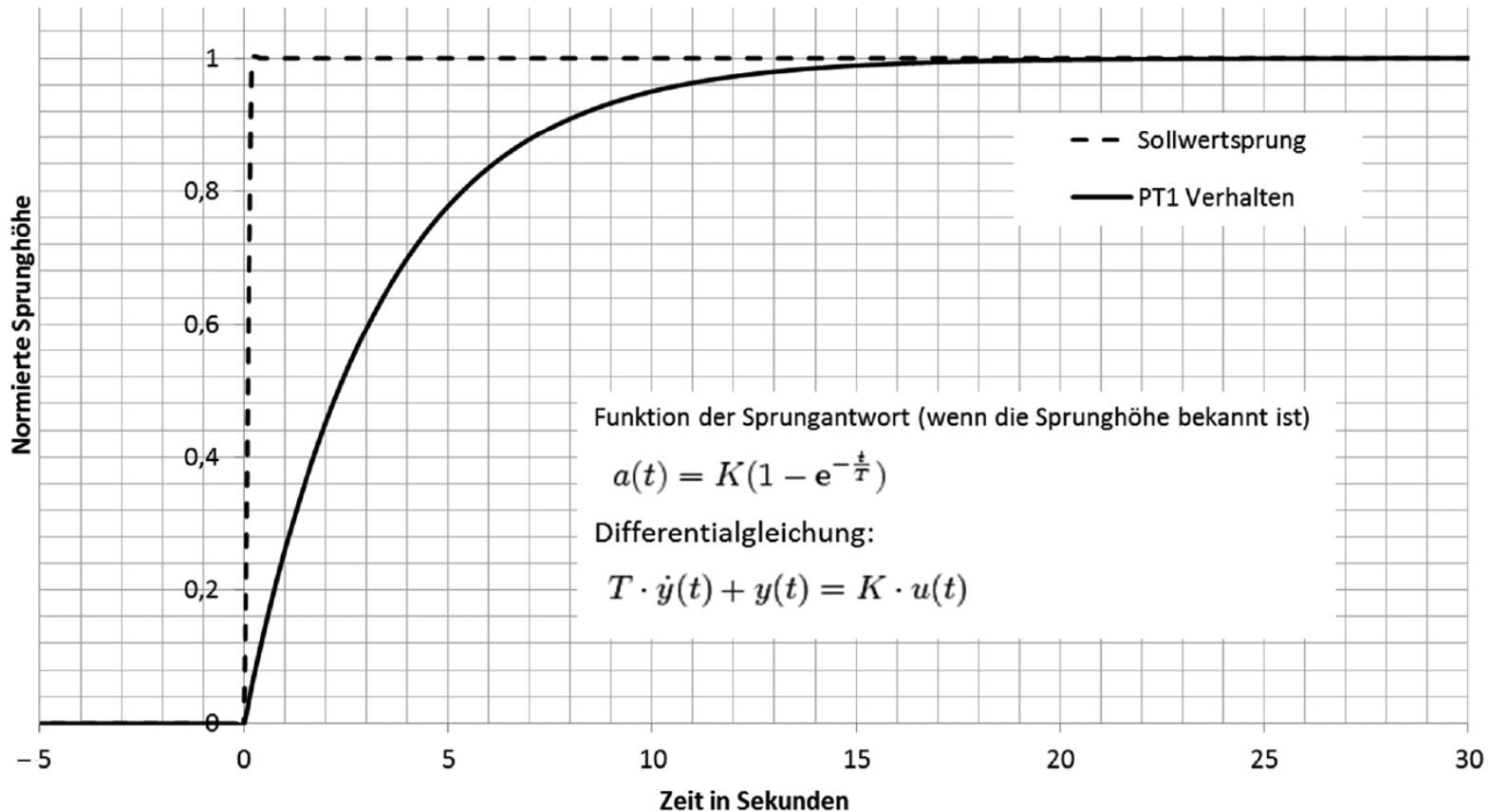
- Requirements for the reactive power capability at partial load  $P_{mom}$
- ( $0.05 < P_{mom} / P_{b\ inst} < 1$ ) at grid connection point
- Maximum residual deviation  $\pm 2.0\ %$  with regard to  $P_{inst}$ , for power generating modules  $< 300\ kVA$  maximum  $\pm 4.0\ %$  with regard to  $P_{inst}$ .
- Reactive power in range  $0 \leq P_{mom} / P_{b\ inst} < 0.05$  no more than  $5\ %$  of sum of stipulated active power supply  $P_{AV, E}$ .

## 10.2.2 Static voltage stability: Procedure for reactive power supply at the grid connection point

- |                                       |   |
|---------------------------------------|---|
|                                       | MV – Directive 2008                         |
| a) Q (U)                              | a) fixed displacement factor $\cos \varphi$ |
| b) Q (P)                              | b) $\cos \varphi$ (P)                       |
| c) Reactive power kvar                | c) fixed reactive power MVar                |
| d) displacement factor $\cos \varphi$ | d) Q (U)                                    |
- Control behavior of reactive power qualitatively according to PT1 – behavior for procedure a), b) and c)
  - Specification of fixed setpoint or variable setpoint via remote control system (or other control technology)
  - Reactive power adjustment of power generating module in range 6 s – 60 s (for 95 % of set point jumps)

Note: Testing of adjustment times by the working group pending

## 10.2.2 Static voltage stability set point jump overall



**Bild 7 – Beispiel des Regelverhaltens bei einem Sollwertsprung mit der Höhe 1 (normiert) und einer Zeitvorgabe (3 Tau) von 10 s**

## 10.2.2 Static voltage stability set point jump with tolerances relevant to analysis

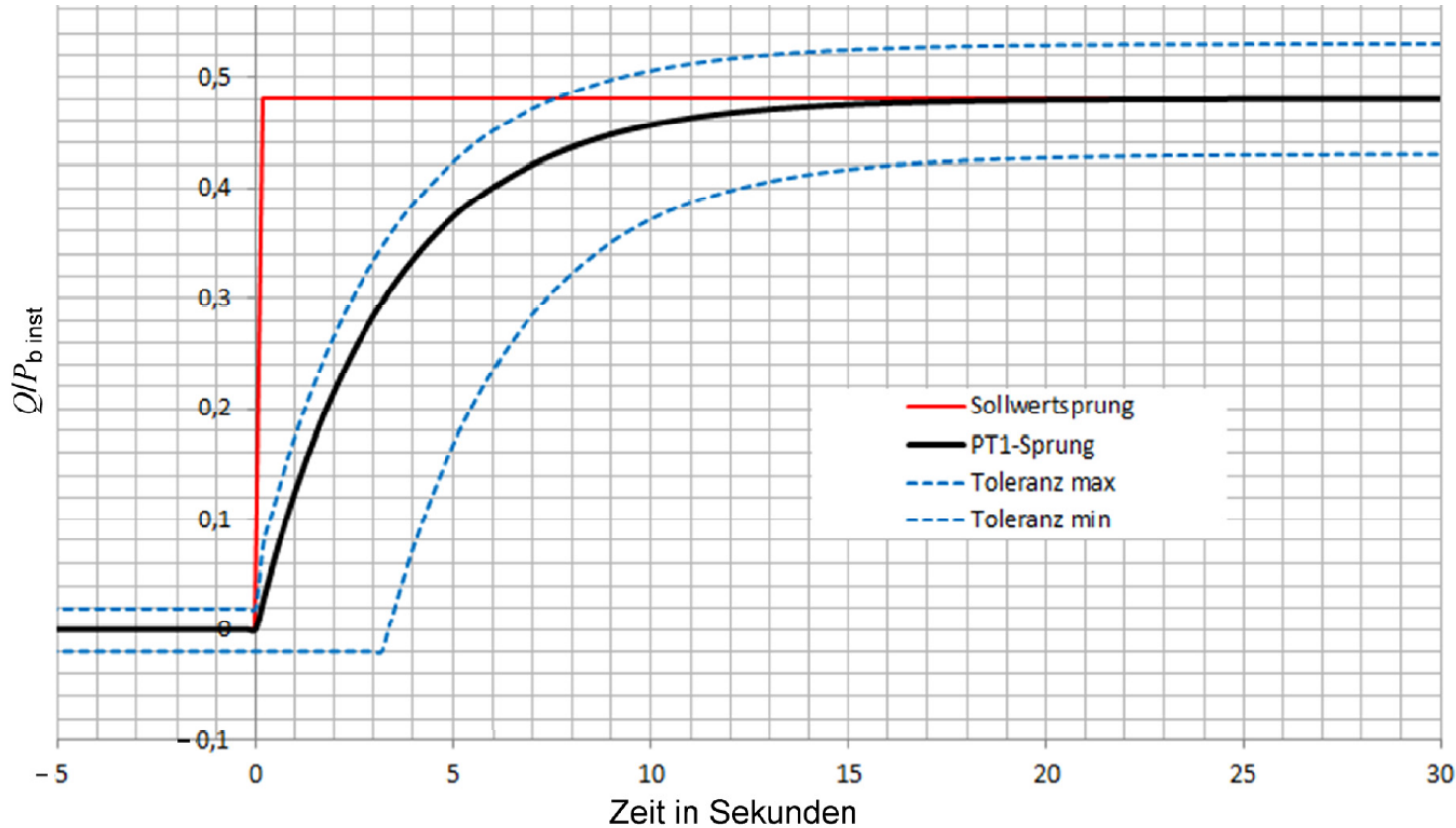


Bild C.3 – Veranschaulichung bei 3 Tau = 10 s

## a) Reactive power – voltage curve Q (U)

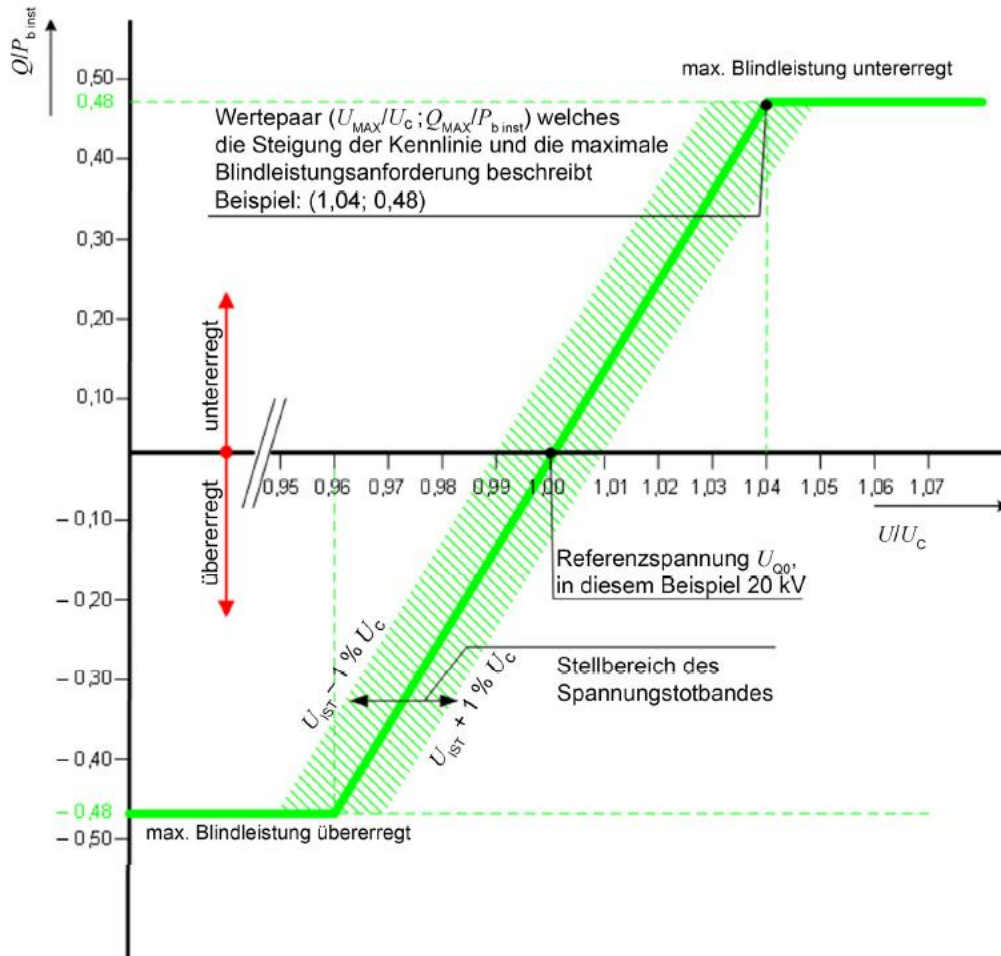


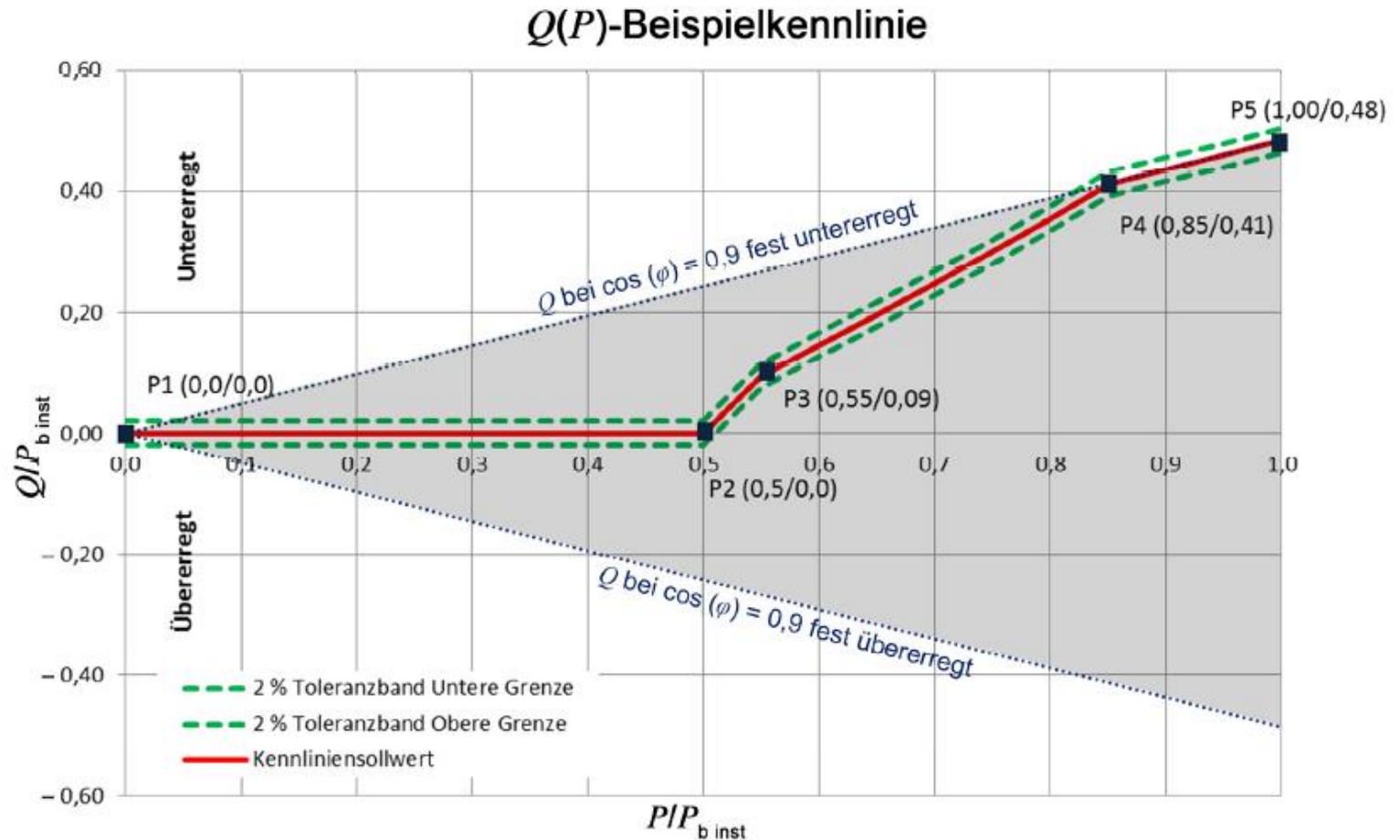
Bild 8 – Beispiel für die Standard-Q (U)-Kennlinie



## a) Reactive power - voltage curve Q (U)

- The curve values are preset (in the course of planning)
- Curve adjustment by grid operator only within reference voltage  $U_{Q0} / U_C$  by remote control technology. I.e. horizontal parallel shift of the curve in 0.5 %  $U_C$  increments.
- Enabling/disabling of Q (U) – curves – control via remote control technology or manually.

## b) Reactive power curve as function of performance Q (P)



**Bild 9 – Beispiel für eine Q (P)-Kennlinie**

## b) Idle power curve as function of performance Q (P)

- Supply of reactive power depending on the current active power supply  
 $Q = f ( P_{\text{mom}} )$
- Curve adjustment via remote control is not foreseen. It will be defined over max. 10 grid points that can be set manually.
- Enabling and disabling of Q (P) – curve by remote control technology (disabled  $\cos \varphi \sim 1$ )

## c) Reactive power

- Supply of reactive power independent of active power supply
- Setpoint in relation to agreed active connection power ( $Q_{EA, \text{ soll}} / P_{b \text{ inst}}$  [%]) termination max.  $1\% P_{b \text{ inst}}$  .
- Setpoints are in range shown by P/Q – diagram (Figure 6)
- Should remote control technology fail ( $> 1 \text{ min}$ ), the default – setpoint of 0 % should be applied, if no value is given by the grid operator.

## d) Displacement factor $\cos \varphi$

- Supply of reactive power to the grid with a constant ratio of active and apparent power.
- Specification of setpoint with minimum steps of  $\Delta \cos \varphi = 0.005$ .
- Maximum fault tolerance of reactive current supply calculated from the fault tolerance of  $\pm 2\%$  or  $\pm 4\%$  in regard to  $P_{b\ inst}$ .
- Grid operator provides setpoint (not provided  $\cos \varphi = 1$ )
- Specification of setpoint possible via remote control technology.
- Reaction time max. 1 min for changes to setpoint.

## 10.2.2.6 Special requirements for combined facilities of generation/demand/storage with demand facilities

- Requirements for the static voltage stability/ reactive power supply for power generating modules and storage must be maintained at the grid connection point.
- Impact of loads is not taken into account
- For reactive power supply  $Q(U)$ ;  $Q(P)$ ; kvar;  $\cos \varphi$ , a simplified solution can be implemented if
  - $P_{inst}$ , installed active power of the power generating module  $\leq 50\%$  of the agreed reference power  $P_{AV, B}$  of the combined facility of generation/demand/storage
  - Agreement of the grid operator

## 10.2.2.6 Special requirements for combined facilities of generation/demand/storage with demand facilities

### Simplified solution

- for  $Q(P)$ ; kvar;  $\cos \varphi$ , the measurement of reactive and active power can be undertaken at the generation unit (with computed correction)
- For  $Q(U)$ , the voltage measurement must be taken at the voltage level of the grid connection point. Shift of the measuring point within the voltage level is possible if  $\Delta U \leq 0.2 \% U_C$ .
- Measurement of reactive power supply at the generation unit.

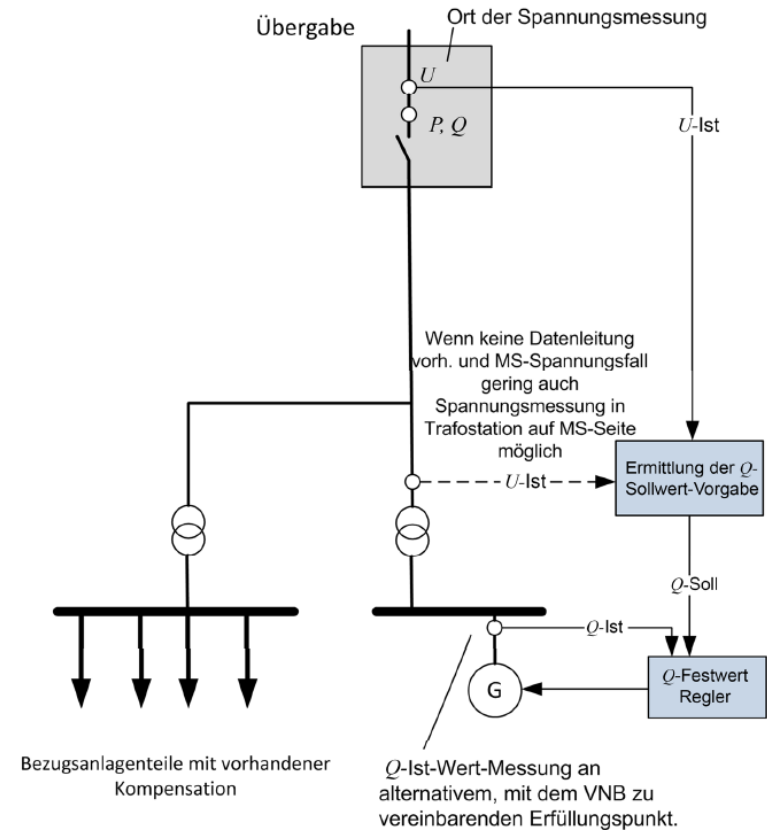


Bild 11 – Beispiel der Erfüllung der  $Q(U)$ -Kennlinien-Regelung an zu vereinbarem Ort bei Mischanlagen

## Section 10.2.3

# Dynamic Grid Support



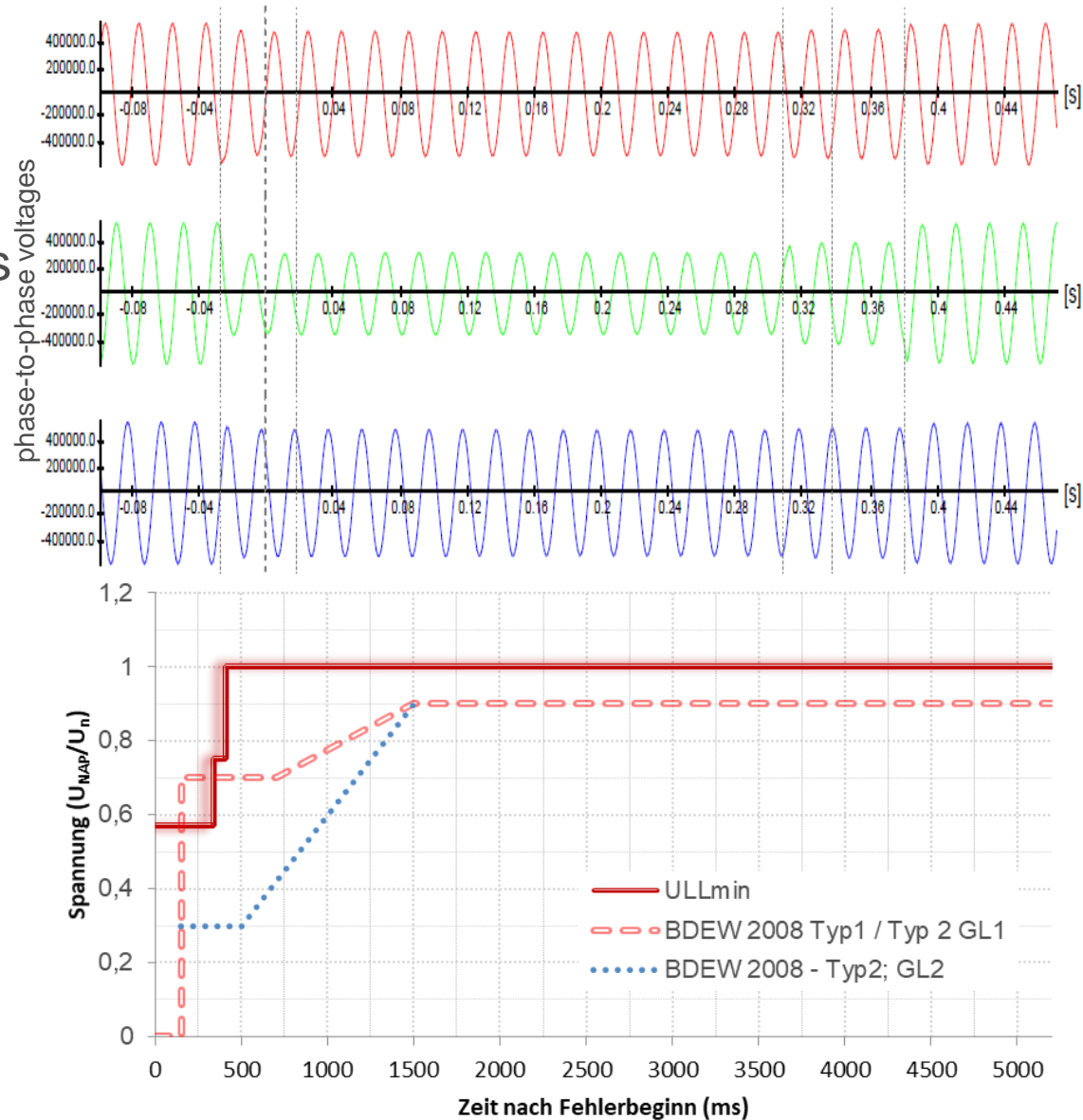
## Outline

- Introduction and brief review of BDEW medium voltage directive
- Draft AR-N 4110 - overview
- Type 1-modules
  - Time constraints
  - Other requirements
  - Multiple faults
- Type 2-modules
  - Fault start / fault end
  - Time constraints
  - Comprehensive and Restricted Dynamic Grid Support
  - Multiple faults
- Behavior after fault end (Type1 and Type 2)

# Introduction with review

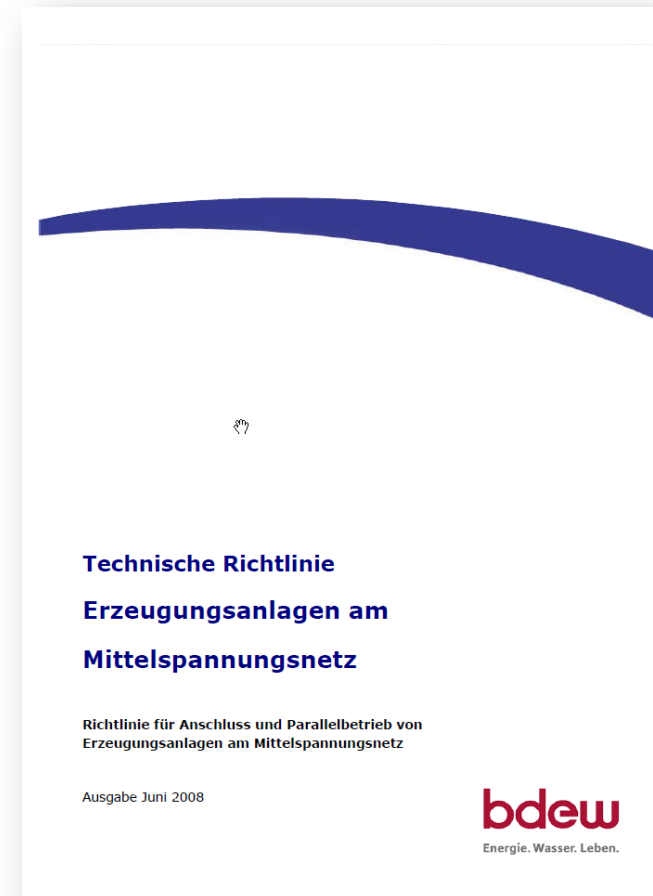
## Motivation

- Example: Two-phase faults in high voltage grid
- max. changes to voltage:  
Positive sequence: 20%  
negative sequence: 21%
- Unsymmetrical faults far more frequent than symmetrical
- Also incorporate fault-remote systems in the voltage support
- Support after the fault, to maintain reactive power allowance



## Status Quo: dyn. grid support in the BDEW medium voltage directive

- Riding through grid faults with defined timed limits
- Supply of a short-circuit current with agreement of the grid operator, in accordance with TransmissionCode 2007 (TC2007)
- Increase in voltage should be limited in non-faulty phases
- Type-2 modules: Temporary disconnection allowed in principle if necessary upon agreement with the grid operator
- Grid support also in the case of repeated Automatic Restart (AR)
- Active power re-establishment min. 10%  $P_n/s$



## Draft AR-N 4110

*Entwurf* März 2017

|  |   |            |
|--|---|------------|
|  | <b>VDE-AR-N 4110</b>  | <b>VDE</b> |
|  | Dies ist eine VDE-Anwendungsregel im Sinne von VDE 0022 unter gleichzeitiger Einhaltung des in der VDE-AR-N 100 beschriebenen Verfahrens. Sie ist nach der Durchführung des vom VDE-Präsidium beschlossenen Genehmigungsverfahrens unter der oben angeführten Nummer in das VDE-Vorschriftenwerk aufgenommen und in der „Liste Elektrotechnik + Automation“ bekannt gegeben worden. | <b>FNN</b> |

**Vervielfältigung – auch für innerbetriebliche Zwecke – nicht gestattet.**

ICS 29.240.01 Einsprüche bis 2017-04-17

**Entwurf**

**Technische Regeln für den Anschluss von Kundenanlagen an das Mittelspannungsnetz und deren Betrieb (TAR Mittelspannung)**

Technical requirements for the connection and operation of customer installations to the medium voltage network (TAR medium voltage)

Exigences techniques pour la connexion et l'opération des installations des clients au réseau à moyenne tension (TAR moyenne tension)

**Anwendungswarnvermerk**

Dieser VDE-Anwendungsregel-Entwurf mit Erscheinungsdatum 2017-02-17 wird der Öffentlichkeit zur Prüfung und Stellungnahme vorgelegt.

Weil die beabsichtigte VDE-Anwendungsregel von der vorliegenden Fassung abweichen kann, ist die Anwendung dieses Entwurfs besonders zu vereinbaren.

Stellungnahmen werden erbeten

- vorzugsweise online im Entwurfsportal des VDE-Verlags unter [www.entwurfe.normenbibliothek.de](http://www.entwurfe.normenbibliothek.de), sofern dort wiedergegeben;
- oder als Datei per E-Mail an [fnn@vde.com](mailto:fnn@vde.com) möglichst in Form einer Tabelle. Die Vorlage dieser Tabelle kann im Internet unter [www.vde.com/fnn-stellungnahme](http://www.vde.com/fnn-stellungnahme) abgerufen werden;
- oder in Papierform an den VDE Verband der Elektrotechnik Elektronik Informationstechnik e. V., FNN, Bismarckstr. 33, 10625 Berlin.

Die Empfänger dieses VDE-Anwendungsregel-Entwurfs werden gebeten, mit ihren Kommentaren jegliche relevanten Patentrechte, die sie kennen, mitzuteilen und unterstützende Dokumentationen zur Verfügung zu stellen.

Gesamtumfang 231 Seiten

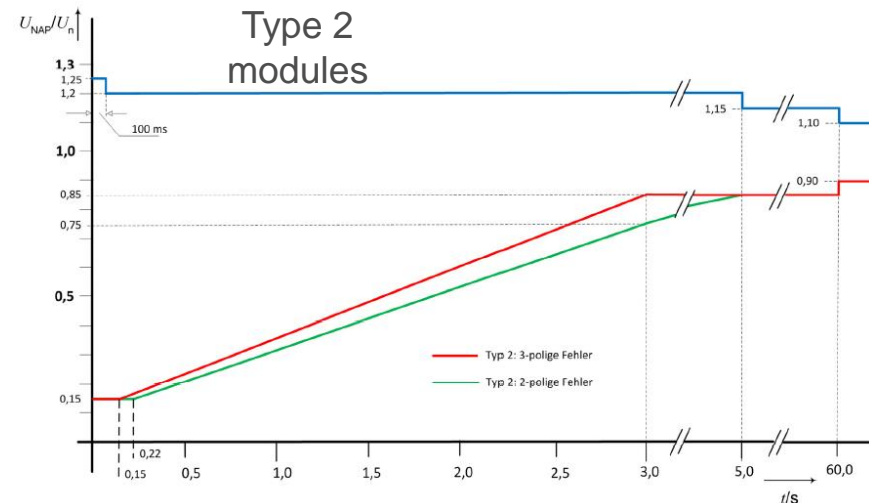
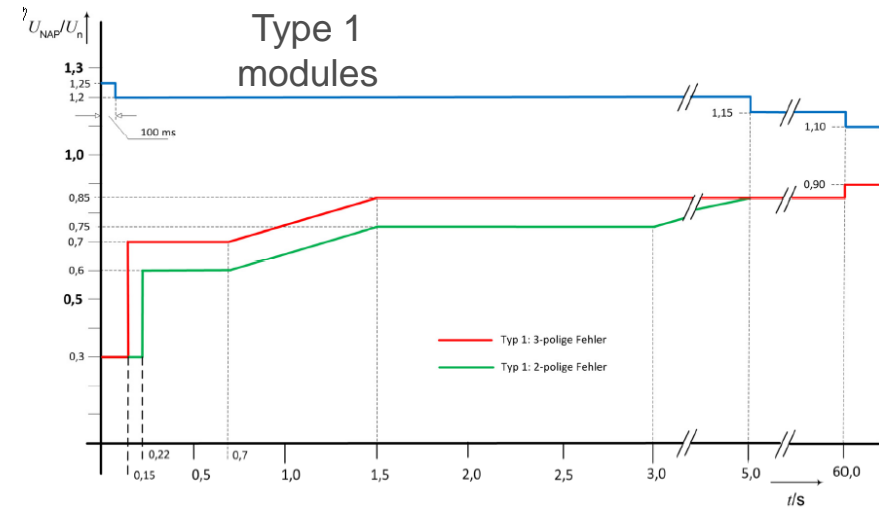
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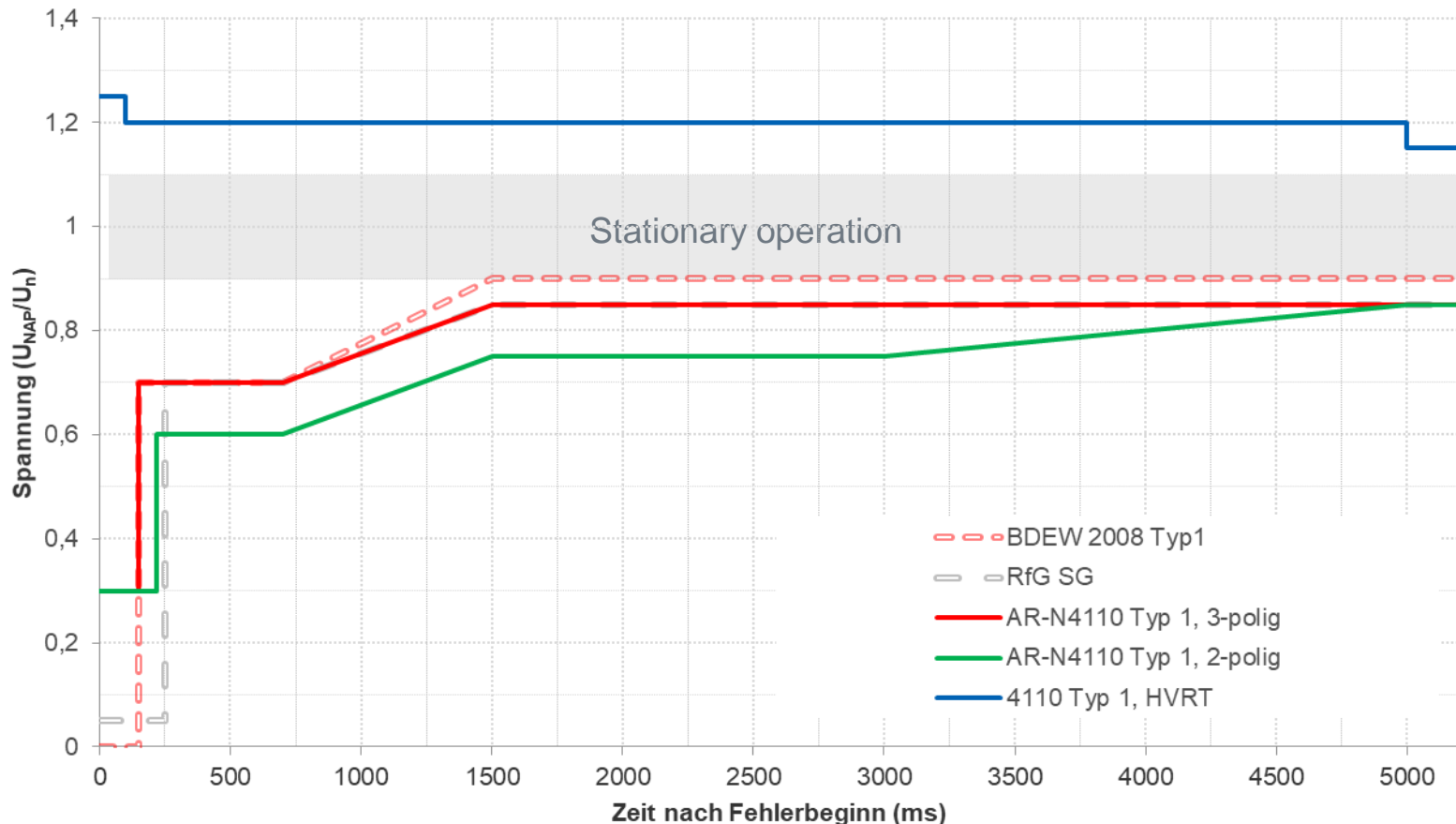
# Dynamic Grid Support for AR-N-4110 - Fundamentals

- power generating modules must ride through *symmetrical and unsymmetrical* grid faults
- to evaluate: smallest/largest of the three *phase-to-phase voltages* on the GCP (half-frequency oscillation RMS)
- Dynamic reactive current support in the *positive and negative sequence*
- Multiple faults* must also be ridden through
- Voltage *surges within* the FRT curves must not lead to tipping



**Type 1 modules  
(directly linked synchronous generators)**

## Type 1 modules: Time constraints



- LVRT requirements were **slightly adjusted** (RfG curve for **symmetrical faults**)
- **Two-phase faults**: often more profound issue, usually non-critical for PGM (green curve)
- New: Requirements for riding through **surges** (HVRT)



## Other / general requirements Type 1 modules

- Voltage drops within the a.m. limit curve should be ridden through if  $S_k$  is  $> 5 S_{A,Ges}$  after end of fault in the relevant grid
- Voltage regulator settings and software status must be defined and traceable
- Maximum voltage increase in the functioning external conductors maximum 5%  $U_C$  compared to pre-fault voltages
- Behavior after fault end  
Increase in active current as quickly as possible, response time maximum 3 seconds

## Multiple faults

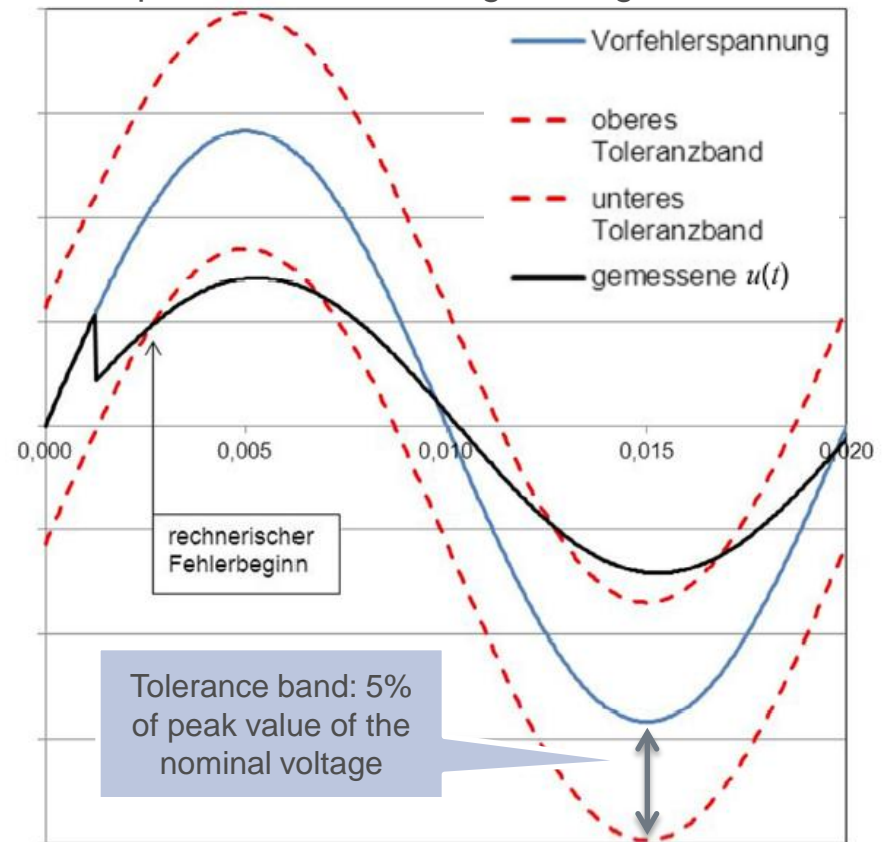
- It must be possible to ride through **multiple consecutive faults**
- **Thermal design** of the generator according to DIN EN 60034-1 must be guaranteed
- Tipping **permitted**, if these thermal limits are **exceeded** due to multiple faults

**Type 2 modules  
generators that do not comply with Type 1**

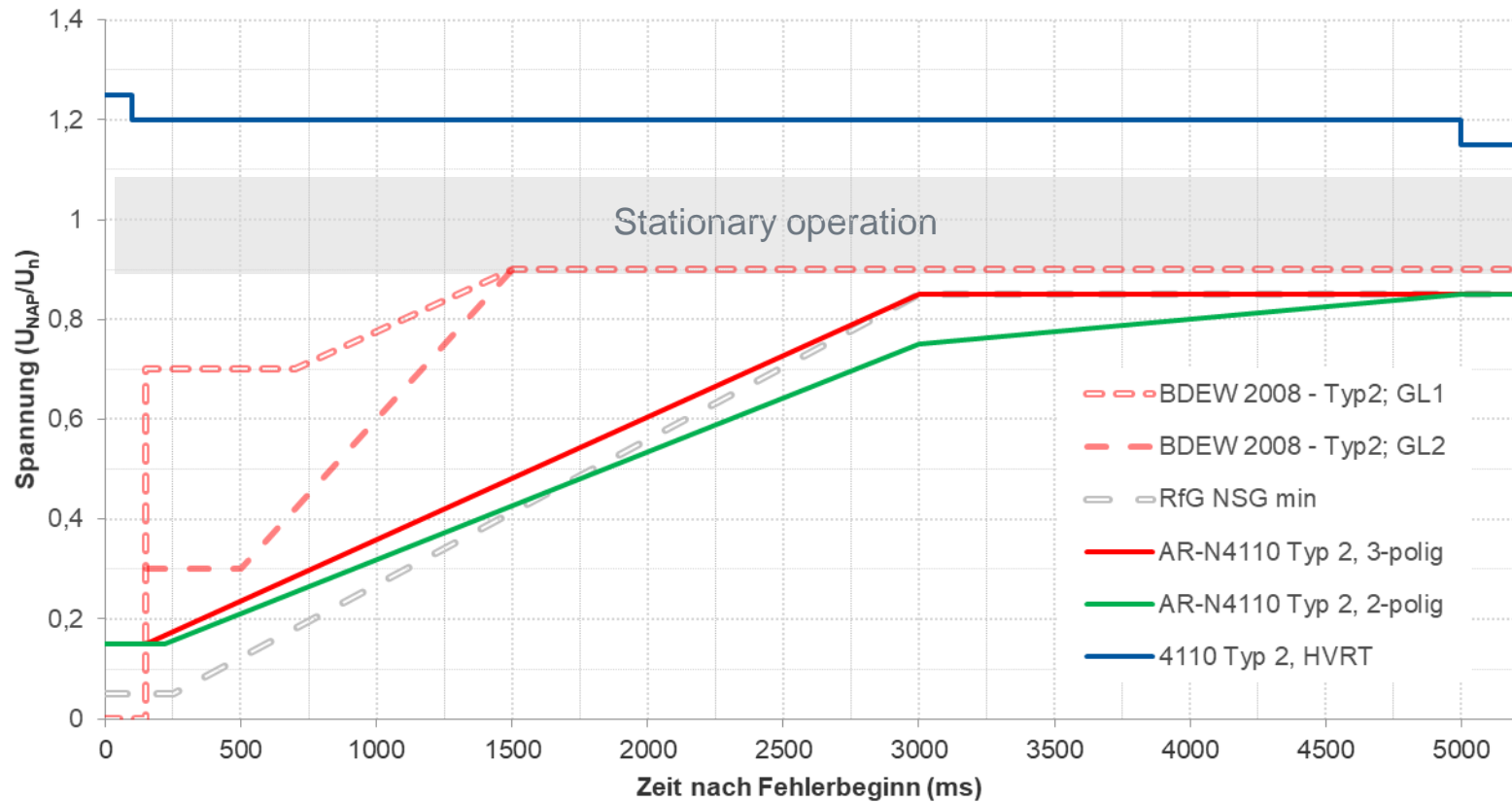
## Type 2 modules: Fault start and end

- Criteria for **fault start**:
  - sudden voltage **changes** compared to 50 pre-fault voltage periods
  - Voltages  $> 1.1 U_C$  [max.  $1.15 U_C$ ] or  $< 0.9 U_C$   
 $U_C$ : Agreed supply voltage, usually equals  $U_n$
- Criteria for **fault end**:
  - 5s after fault start
  - Restoration of all L-voltages in the range of  $0.9 U_C < U < 1.1 U_C$
- **New** faults, as soon as a criterion for fault end is completed

Example of a sudden voltage change



## Type 2 modules: Time constraints



- Requirements of Type 2 modules **expanded**, to conform to RfG limit curve
- **Two-phase faults**: often more profound issue, usually non-critical for EZA (green curve)
- New: Requirements for riding through **surges** (HVRT)

## Type 2 modules: Comprehensive Dynamic Grid Support

- Supply of an additional reactive current from fault start (standard configuration, if not explicitly stated otherwise)
- Objective: Optimum grid support for **symmetrical and unsymmetrical** faults
- Minimization of surges in non-faulty phases → **grid support in positive and negative sequence**
- Voltage measurement and provision of additional reactive current at the **PGU**
- Reactive current is prioritized
- After **fault end**:  
Increase in active current to pre-fault value within **maximum one second (response time)**

## Type 2 modules: Comprehensive Dynamic Grid Support

- Context: 1 min mean value for the grid voltage ( $U_2 \rightarrow 0$ )  
 $\rightarrow$  unchanged reference for the whole duration of the fault

$$\Delta u_1 = \frac{U_1 - U_{1min}}{U_C}$$

$$\Delta u_2 = \frac{U_2}{U_C}$$

- zus. Blindstrom:

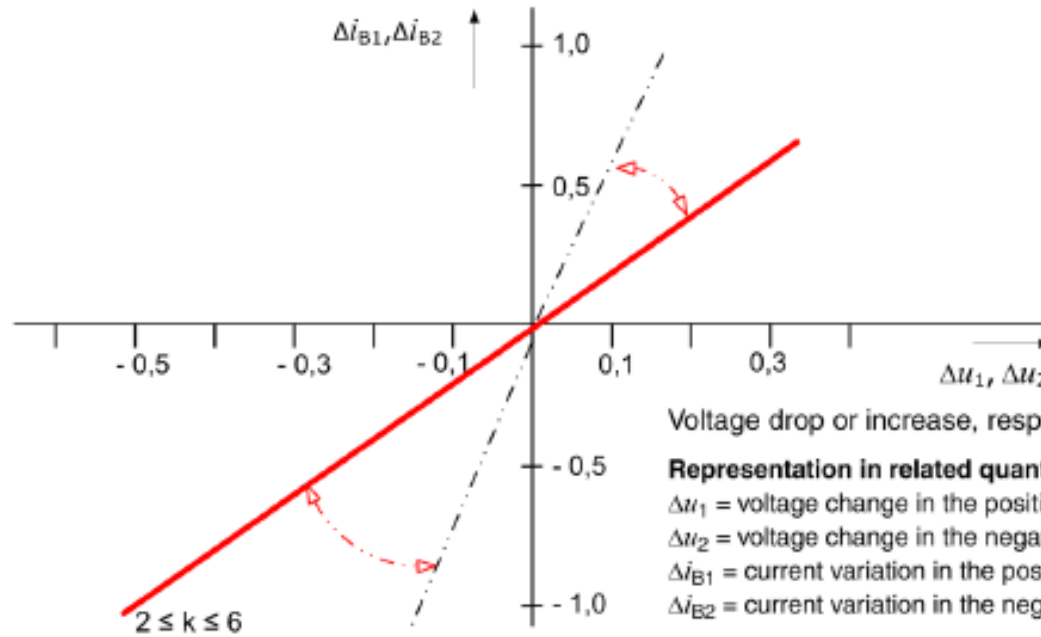
$$\Delta i_{B1,2} = k \cdot \Delta u_{1,2}$$

- Dynamik:

$$T_{an_{90\%}} \leq 30 \text{ ms}$$

$$T_{ein_{\Delta x}} \leq 60 \text{ ms}$$

Additional reactive current required



Voltage drop or increase, respectively

**Representation in related quantities:**

- $\Delta u_1$  = voltage change in the positive sequence system
- $\Delta u_2$  = voltage change in the negative sequence system
- $\Delta i_{B1}$  = current variation in the positive sequence system
- $\Delta i_{B2}$  = current variation in the negative sequence system

## Restricted Dynamic Grid Support

- Intermediate supply to the grid through comprehensive dynamic grid support can limit the **effectiveness of an Automatic Restart (AR)**
- Therefore: Grid operator can request that grid faults are ridden through **without current supply**
- Criterion for **fault start**:  $U < 0.8 U_C$
- For voltage surges above this limit: undertake comprehensive dynamic grid support



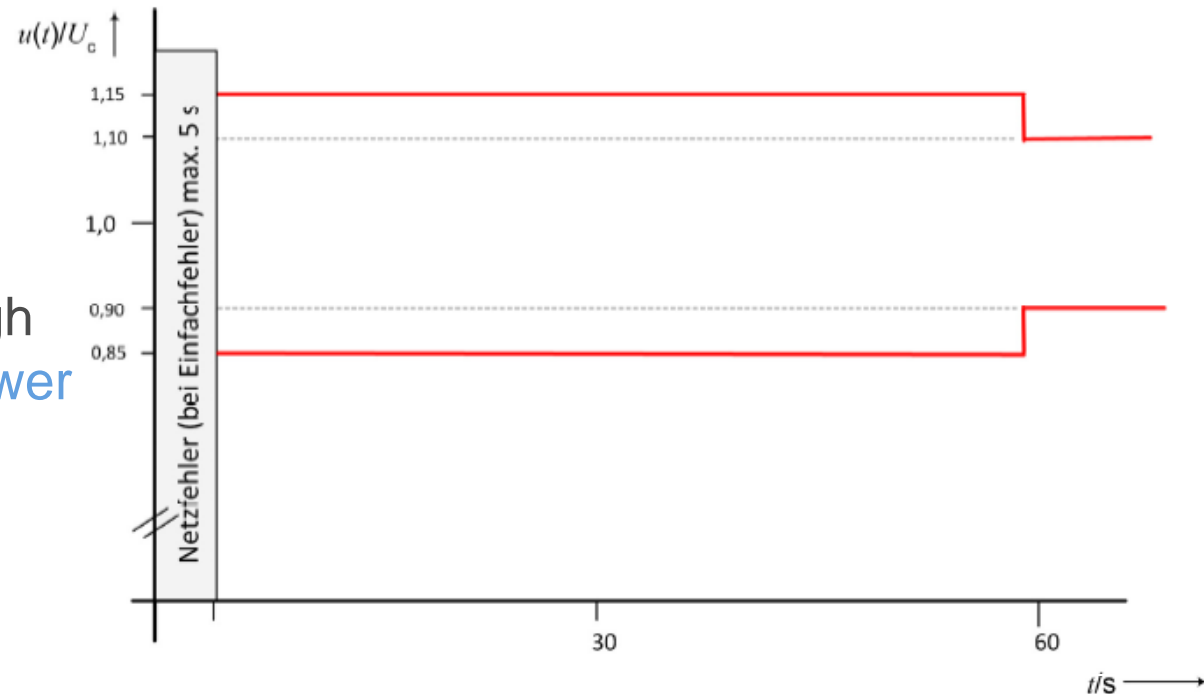
## Multiple faults

- It must be possible to ride through an **arbitrary sequence** of grid faults
- For some plant types, limitation is possible (e.g. thermal limits with the use of choppers)
  - Requirement is limited to the energy to be removed or not supplied to the grid of  $P_{E_{max}} \cdot 2s$
- between multiple grid fault sequences, a time of **30min** is estimated

# Behavior after fault end (Type 1 and Type 2)

## Conduct between fault endings and stage. Plant (Type 1 & 2)

- after fault end, the grid voltage is possibly still outside the range  $U_C \pm 10\%$  until the HV/MV transformers stepping switch re-adjusts
- modules may still have to supply a reactive current, to prevent a triggering of the protection mechanisms
- possible support through adaptation of active power



## Summary

- Requirements of AR-N 4110 for dynamic grid support are more extensive than previously and were aligned with the RfG framework
- The required conduct was specifically defined regarding:
  - unsymmetrical faults
  - definition of fault start / end for Type 2 modules
  - conduct after the fault
  - dynamic
  - Multiple faults

## Section 10.2.4

### **Active Power Supply**

## Requirements for power generating modules – active power supply

- 10.2.4.1 Overview
  - Speed restrictions
  - Prioritisation
- 10.2.4.2 Grid security management
  - DSO requirements
  - Implementation for combined facilities of generation/demand/storage
- 10.2.4.3 Active power supply for over or under frequency
  - Requirements of grid retention
  - P-f curve

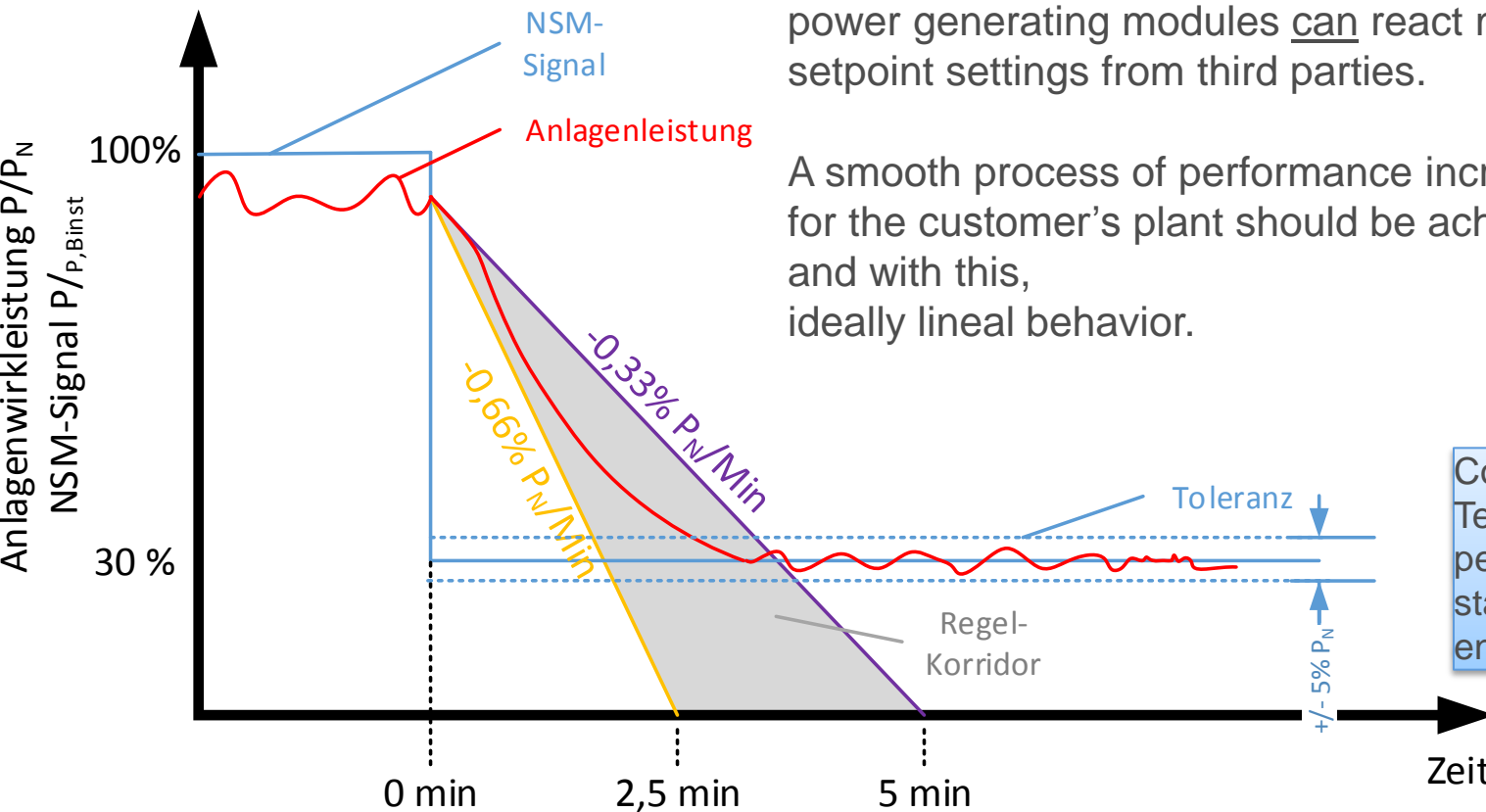
## PGM – active power supply / overview

- Challenges:
  - increasing number of plants participate in direct marketing
  - higher power gradients up to 15 min change as a result
  - sudden power changes are always dangerous
  - synchronized plant behavior potentially critical
  - with system performance, “many cooks” are increasingly involved.
  - also for surface circuits by DSO (cascade), a greater change to performance is required.
  - in future, controllable demand facilities are also likely

## PGM – active power supply / limitation of gradients

Limitation of performance gradients are for increasing and reducing active power supply and active power usage

- no faster than in 2.5 min ( $0.66\% P_N$  per second);
  - no slower than in 5 min ( $0.33\% P_N$  per second).
- power generating modules can react more slowly to setpoint settings from third parties.



A smooth process of performance increase or reduction for the customer's plant should be achieved, and with this, ideally lineal behavior.

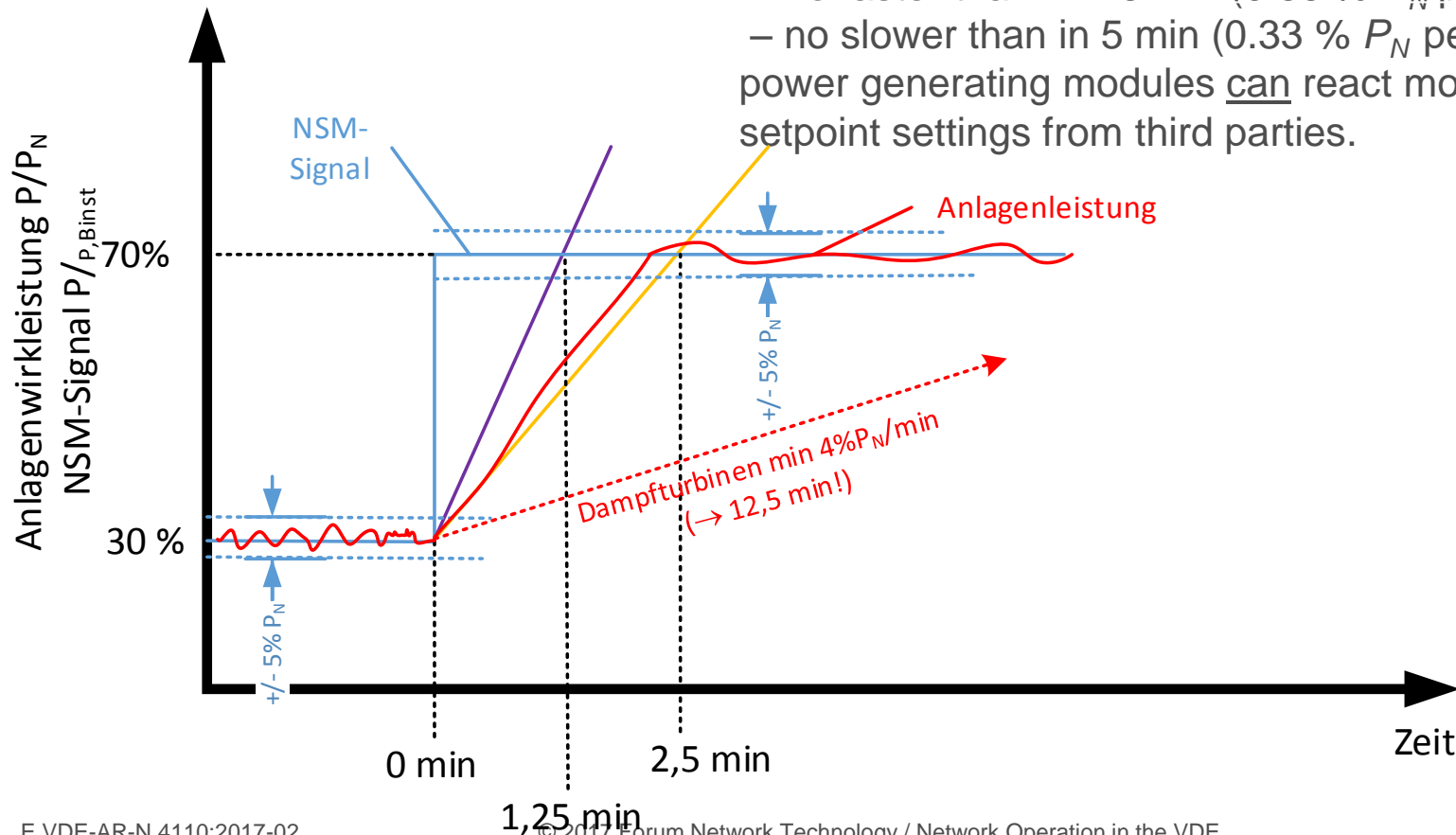
Comments:  
Techn. minimum performance stated for combustion engines



## PGM – active power supply / performance increase

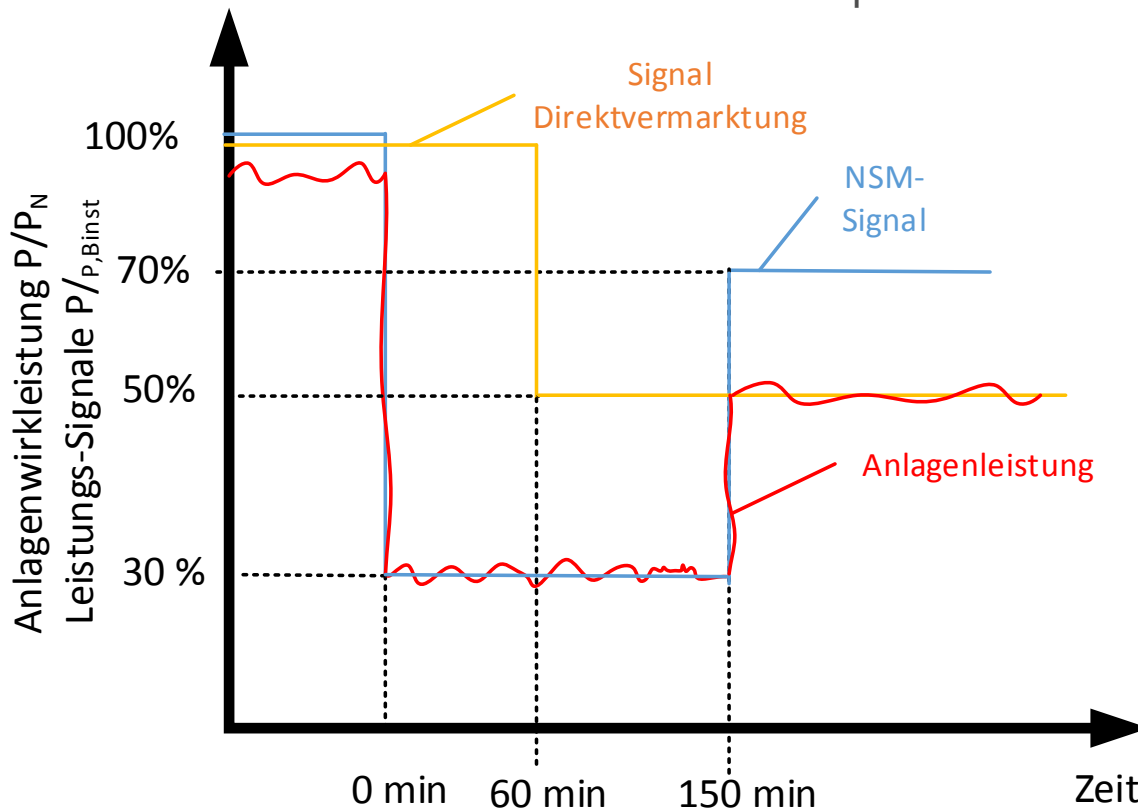
Limitation of performance gradients are for increasing and reducing active power supply and active power usage

- no faster than in 2.5 min (0.66 %  $P_N$  per second);
  - no slower than in 5 min (0.33 %  $P_N$  per second).
- power generating modules can react more slowly to setpoint settings from third parties.



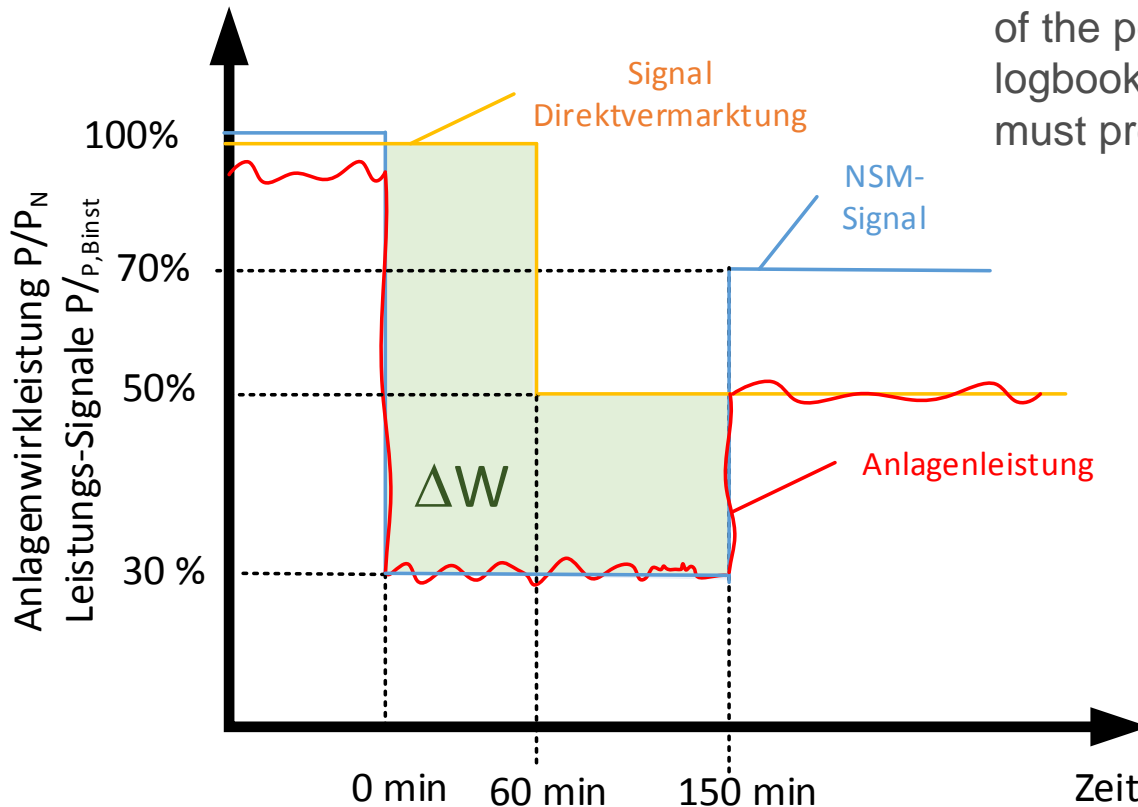
## PGM – active power supply / priority regulations

With temporally overlapping active power specifications of grid operators (grid security management) and third parties (market specifications, personal requirement improvements etc.), smaller services always matter



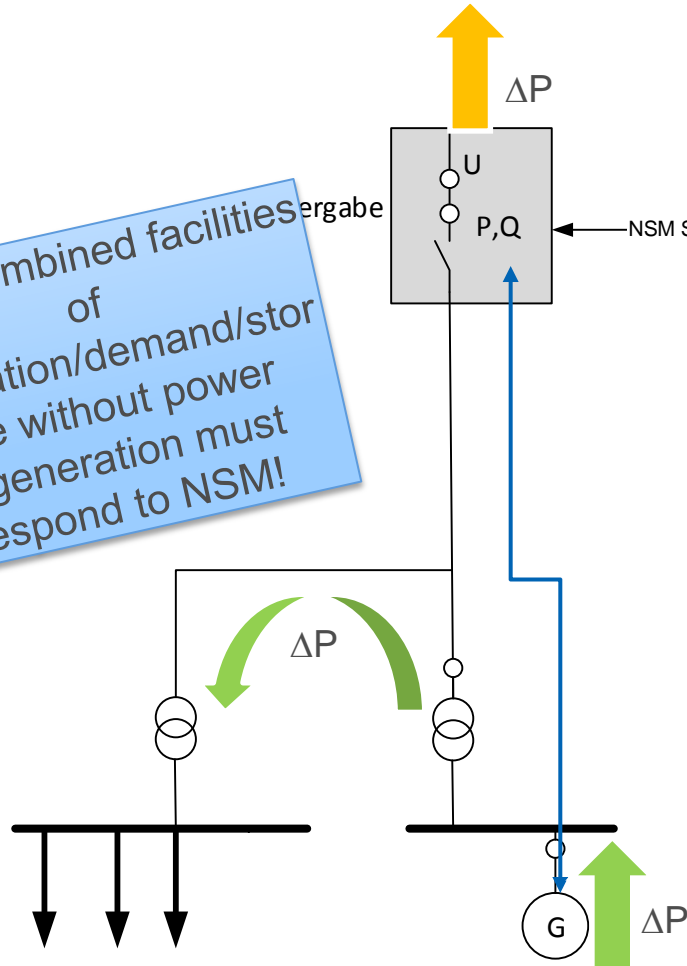
## PGM – active power supply / logbook

The plant operator must always retain evidence for the prior 12 months of power regulation for grid security management and interference by third parties during operation of the power generating module (e.g. in a logbook). Upon demand, the grid operator must present this evidence.



## PGM – active power supply / combined facilities of generation/demand/storage

Even combined facilities of generation/demand/storage without power regeneration must respond to NSM!



Reference value NSM is  $P_{\text{binst}}$

→ Signal independent of instantaneous power

→ Can be directly switched to PGU/PGM. (simple standard case)

Could an (appropriate) load setting instead of a “reduction” also occur?

→ Technically OK; providing “grid power” at GCP is **guaranteed**.

Problem: Evidence management

→ Requirement that  $\Delta P$  must be metrologically traceable

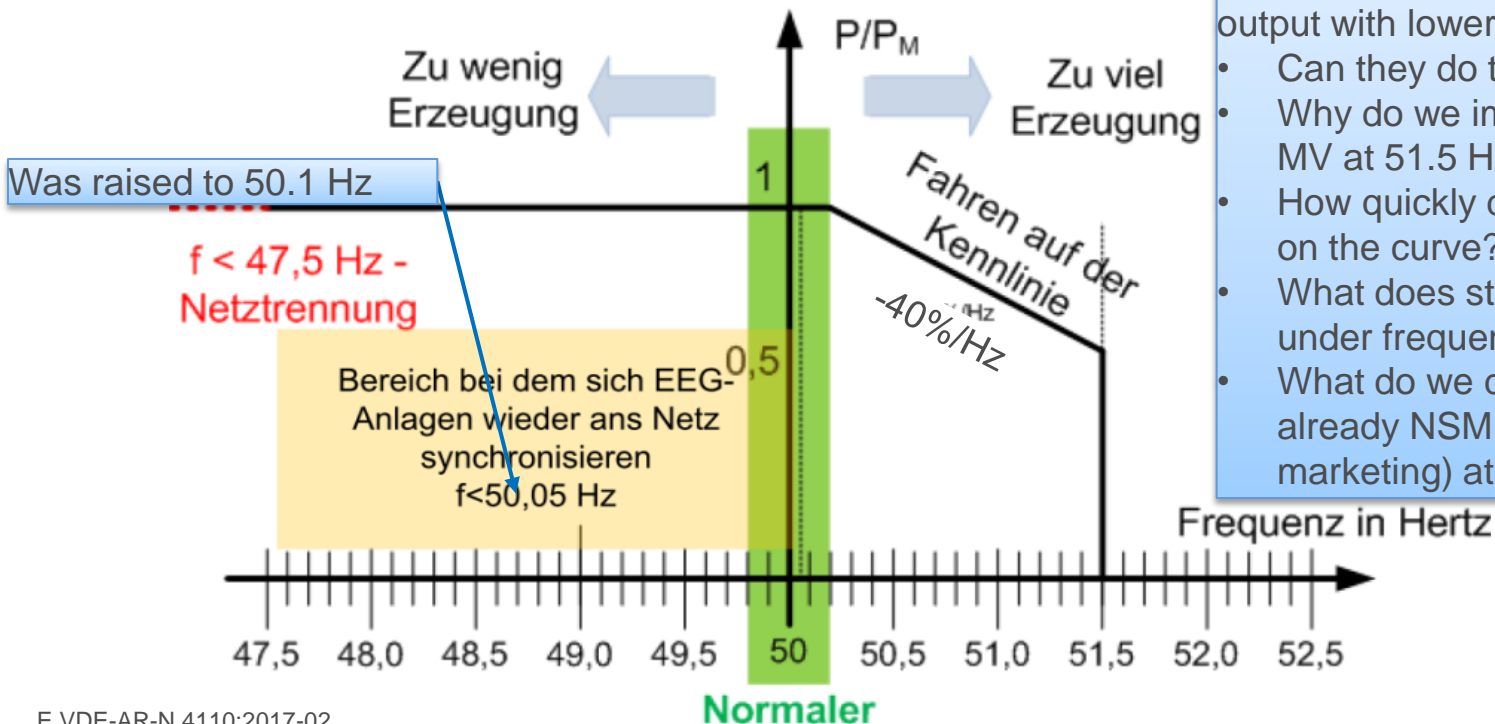
## PGM – Active power supply for over/under frequency

- Frequency: Primary value
  - (integrated grid / SYSTEM / Cross-Border Issue)
  - entso-e values must be observed (Rfg: generator > 0.8 kW = Significant Grid User)
  - 50.2 Hz problem & P-f curve known (Basis)

### Questions:

Turbines & combustion engines reduce output with lower revolutions.

- Can they do that?
- Why do we immediately switch off in MV at 51.5 Hz?
- How quickly do the modules operate on the curve?
- What does storage actually do at under frequency?
- What do we do with market or already NSM limited modules (e.g. marketing) at  $f < 49.8$  Hz?



## Active power supply during frequency deviations

**Fundamentals**

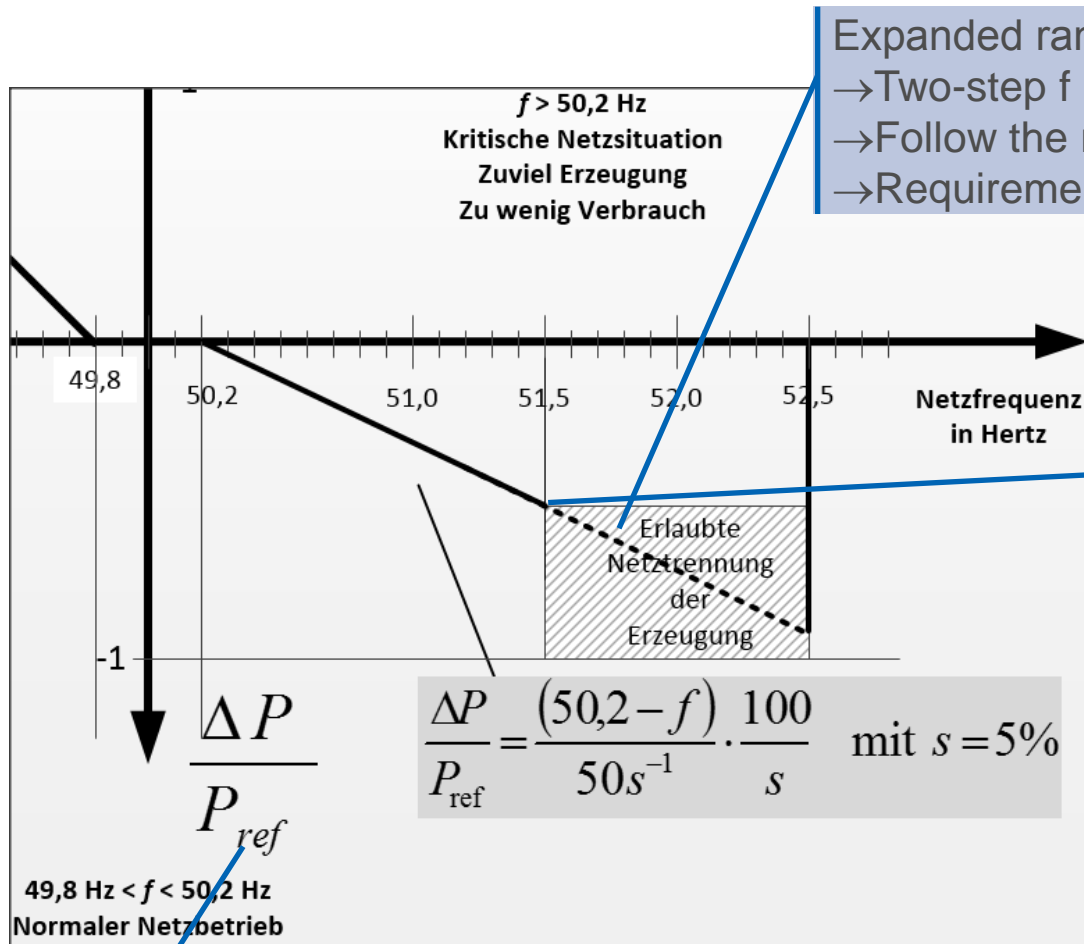
- if  $f < 49.8 \text{ Hz}$  or  $f > 50.2 \text{ Hz}$  then: System is at risk
  - P-changes have priority over market (complies with EnWG Art.13)
  - P-changes do not have priority over NSM

Reason: if NSM was used, the grid is close to 100% capacity at the MV level; additional capacity increase risks tripping protection and a loss of the entire production.

- When does that cease?
  - If  $49.8 \text{ Hz} < f < 50.2 \text{ Hz}$  → generally OK;
  - But please slowly return to “Normal status”!
  - If  $f$  is in “Range”: Active power changes of a maximum of  $10 \% P_N / \text{min}$
  - if  $f$  over 10 min long within the tolerance range → normal grid operation

Most recently:  
2006

## Active power supply at over-frequency



Expanded range for "overshots" by 5 sec.  
 → Two-step  $f >$  protection  
 → Follow the range curve where possible  
 → Requirements not (yet) compulsory

Control times according to Entso-e Rfg:  
 "As fast as technically feasible"

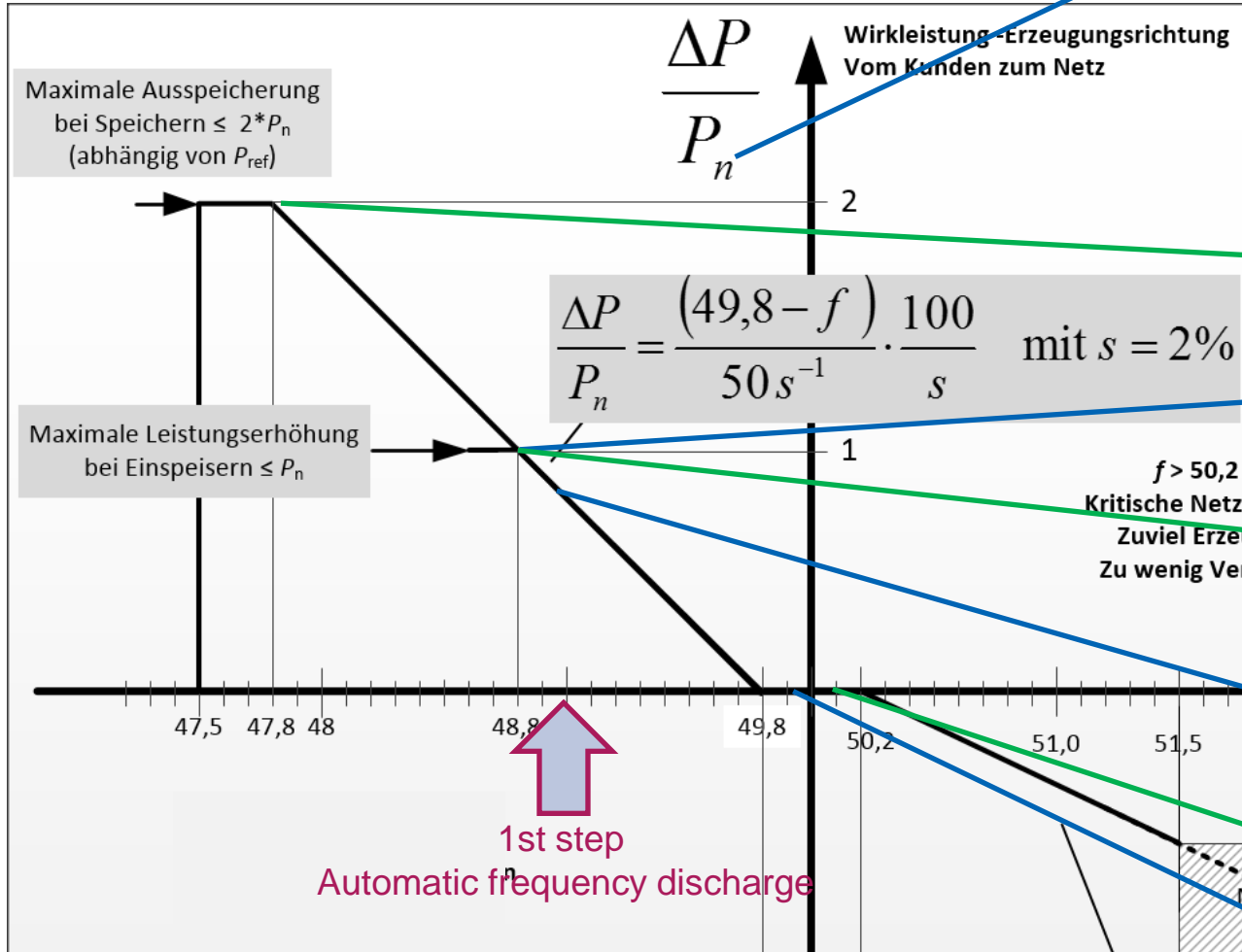
→ As fast as possible  
 → Precision comes second

Response time: 2s  
 Settling time 20s  
 Measuring tolerance < 10 mHz  
 P deviation +/- 10% $P_N$

$P_{ref} = P_{MOM}$  for Type 2: → No change (remains locked at  $f=50.2$  or  $f=49.8$ )  
 $P_{ref} = P_N$  for Type 1: → RfG (fixed curve slope)

## Active power supply at underfrequency

Caution!  
Different axis scaling!  
DP refers to the NOMINAL  
output



Example 1:

Example 2:

$\Delta P = -200\%$   
Storage no longer  
discharges;  $P = -100\%$

$\Delta P = 100\%$   
Storage charges;  $P = -20\%$

$\Delta P = 100\%$   
Storage no longer  
discharges;  $P = -100\%$

$\Delta P = 80\%$   
Storage no longer  
discharges;  $P = 0\%$

Storage is off 0 %

Storage charges at 80 %



## P-f requirements

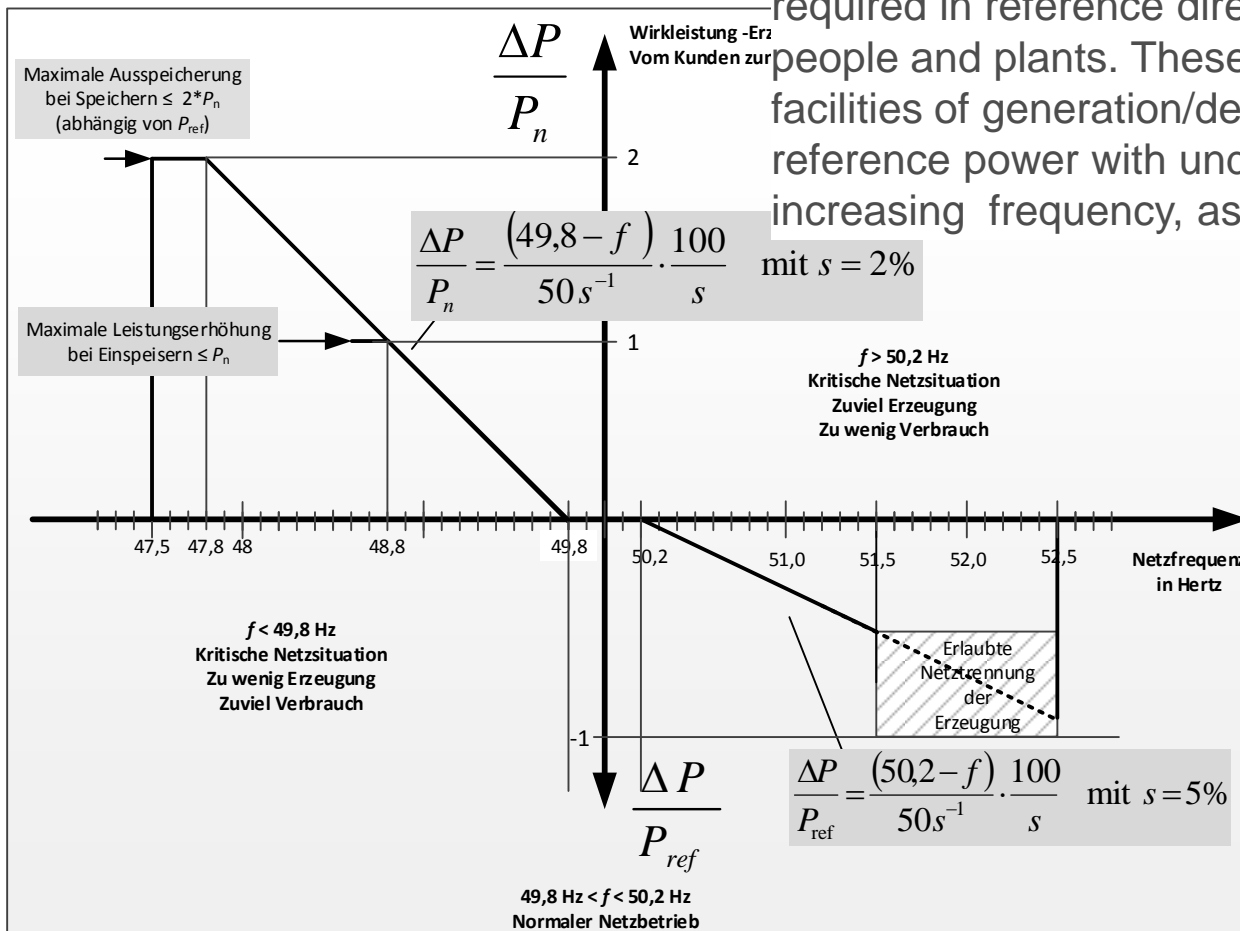
**ΔP requirement! (Direction change is always correct)**

Applies to generators (with storage capacity  $W > P_N \cdot 30s$ )

Applies to applications according to Art. 14 EnWG with electronic control (e.g. load applications for storage or electronically controlled electro-thermal applications)

required in reference direction, providing there is no risk to

people and plants. These demand facilities or combined facilities of generation/demand/storage should lower the reference power with under frequency or increase it with increasing frequency, as shown in Figure 17.



## P-f requirements - control times

### Limited requirements due to technical restrictions

- Wind: Increase only when wind > 50%  $P_N$
- Combustion engines:
  - $\leq 2$  MW minimum 66 %  $P_n$  per minute
  - > 2 MW minimum 20 %  $P_n$  per minute
- Increase through steam turbines; minimum 4 %  $P_n$  /min
- For hydroelectric power plants, a response time of 15 s and a settling time of 30 s is necessary.
- Evidence management in and response times relating to  $\Delta f = 500$  mHz

Control times according to Entso-e Rfg:

“As fast as technically feasible”

-> as fast as possible

-> precision comes second

Storage:

Response time: 2s

Settling time 20s

Measuring tolerance < 10 mHz

P deviation +/- 10% $P_N$

(still) no firm requirements for the  $f <$  range with PGM:

The more who participate now, the sooner it will be possible to make exceptions later

-> The fewer who participate now, the stricter the subsequent directive will be

## Ch. 6.3.3 Protection technology (general)

**For purchasers and for power generating modules**

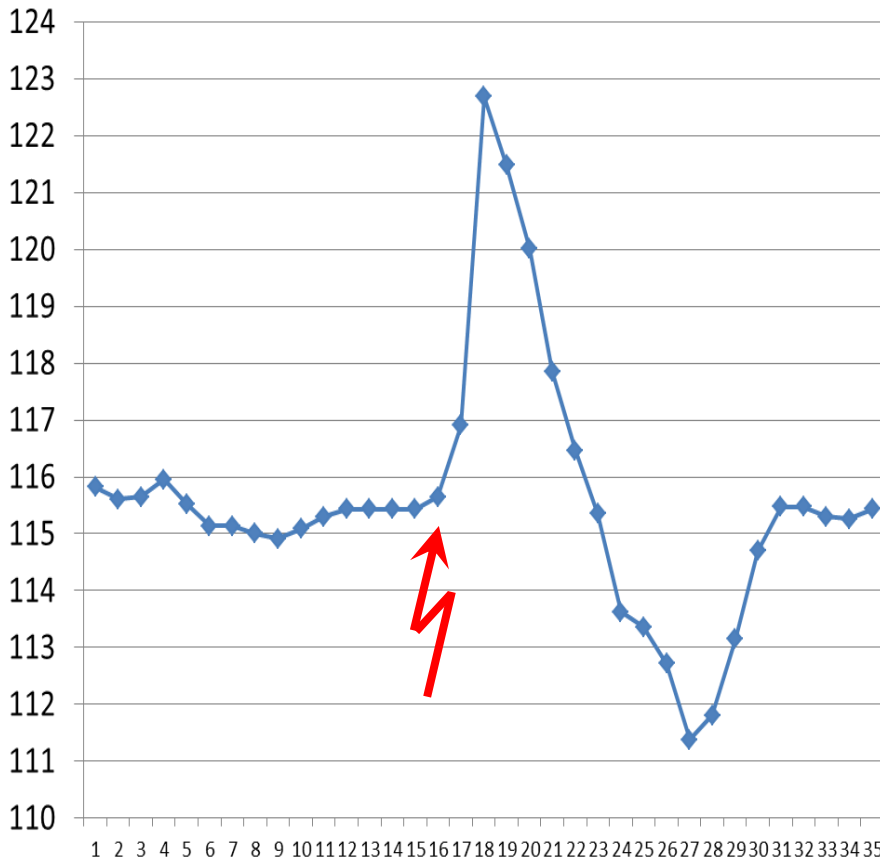
- Applies to demand facilities and to power generating modules, i.e. for
  - grid protection systems
  - the subscriber's short-circuit protection systems and
  - disconnection protection systems (for power generating modules)
- Responsibility lies with the respective owner
- The grid operator can request the installation of a frequency relay and provide the settings for this
- Regular protection inspections are mandatory
- For this, at least one testing terminal bar must be installed
- In justified cases, disturbance recorders must be installed at the grid connection point (e.g., if no metrological evidence of compliance with grid support is available)
- All information necessary for fault investigation must be exchanged between the grid operator and the subscriber.

## Ch. 10.3 Protection systems and protection settings (for power generating modules)

**Experience gained from grid faults with voltage protection systems**

## Case 1) short circuit in 110kV grid

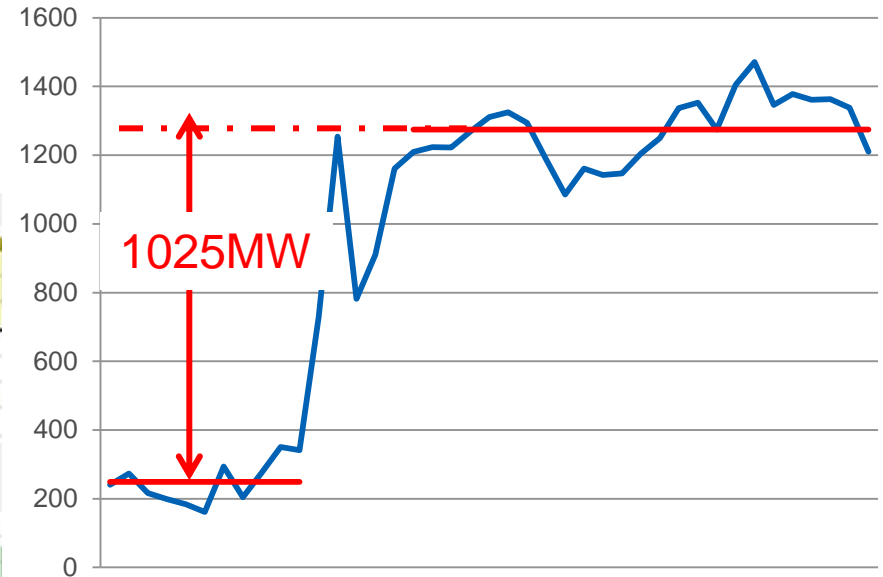
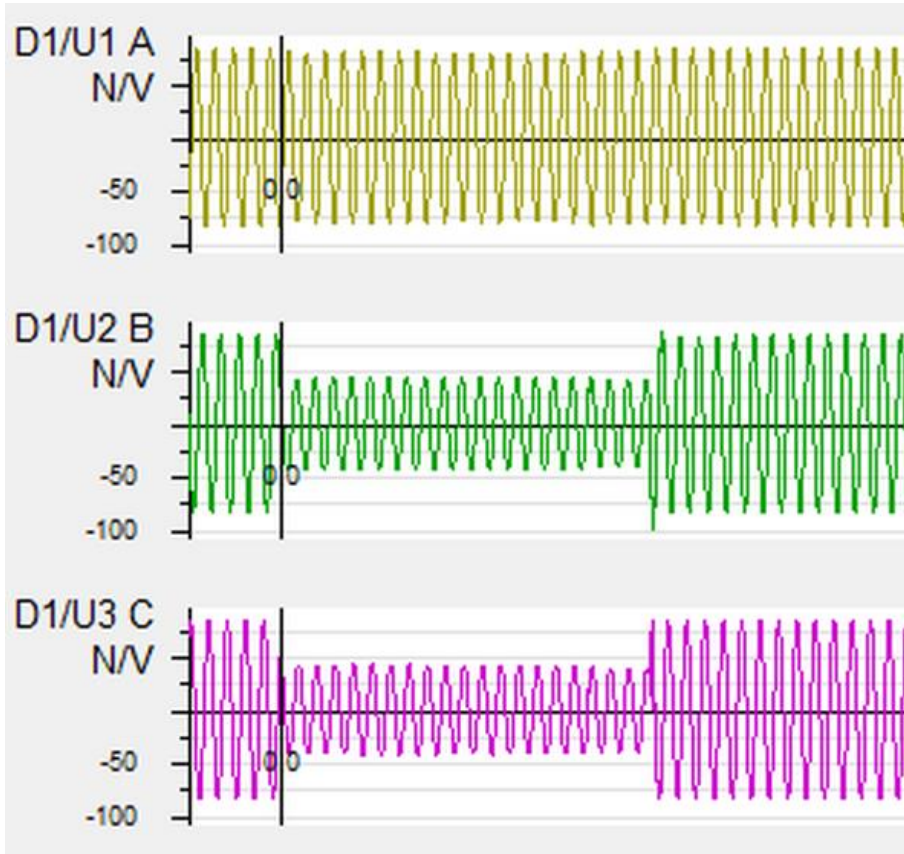
L-L voltage in kV (minute values)



- Two-phase short circuit 110kV
- fault clearing time 90ms
- Loss of generation capacity >900MW
  
- Suspected cause: Response by surge protection systems

\*) source: Effects of grid disruption on energy balance and voltage maintenance, T. Henning, U. Welz, H. Kühn SuL 2014

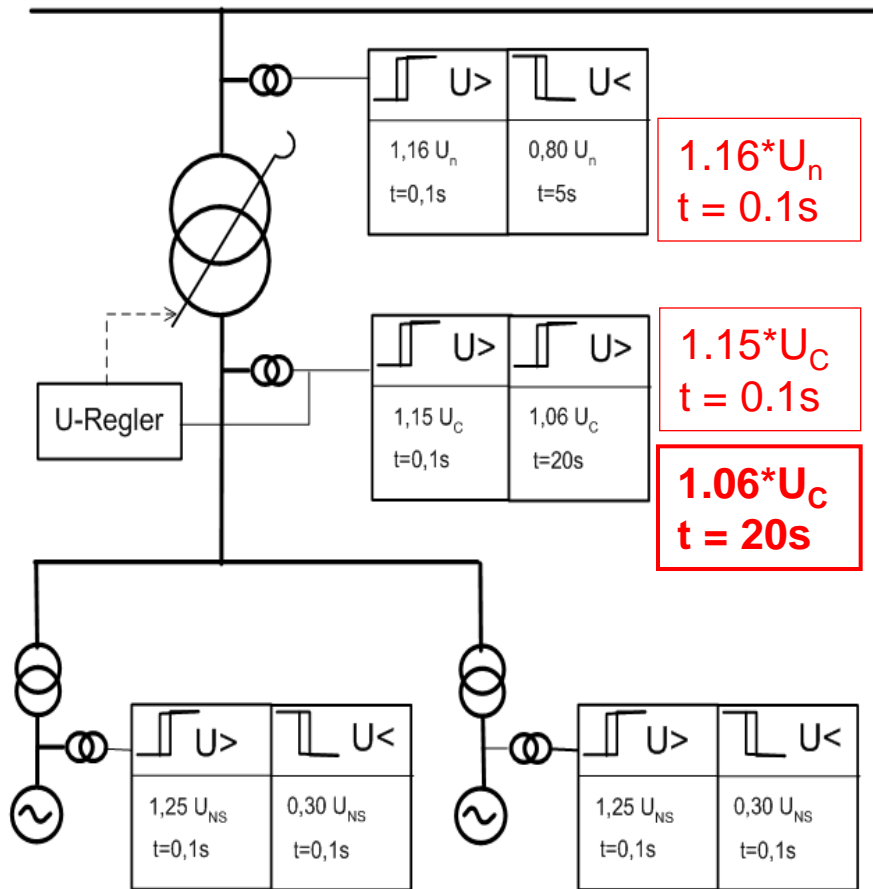
## Case 2) Two-phase short circuit in 380kV grid



- Two-phase short circuit 380kV
- fault clearing time approx. 400ms
- Loss of over 1000 MW
- Suspected cause: Response by surge protection systems

\*) source: Effects of grid disruption on energy balance and voltage maintenance, T. Henning, U. Welz, H. Kühn SuL 2014

## Suspected cause for the loss of generation capacity



- Example formulation of voltage relay  
VDN guidelines from 2004

\*) source: Effects of grid disruption on energy balance and voltage maintenance, T. Henning, U. Welz, H. Kühn SuL 2014



|                       | BDEW 2008   |           | VDE-AR-N 4110         |          |
|-----------------------|---|-----------|-----------------------|----------|
| <b>Function - GCP</b> | Can be omitted by connection to MV grid, if no dynamic grid support is required |           | Always available      |          |
| Voltage increase U>>  | 1,15 U <sub>C</sub>   | 0,1 s     | 1,20 U <sub>MS</sub>  | 0,3 s    |
| Voltage increase U>   | 1,08 U <sub>C</sub>   | 60 s      | 1,10 U <sub>MS</sub>  | 180 s    |
| Voltage decrease U<   | 0,80 U <sub>C</sub>   | 2,7 s     | 0,80 U <sub>N</sub>   | 2,7 s    |
| QU protection Q→&U<   | 0,85 U <sub>C</sub>   | 0,5 s     | 0,85 U <sub>N</sub>   | 0,5 s    |
| <b>Function – PGU</b> | Connection to busbars   |           | Connection to busbars |          |
| Voltage increase U>>  | 1,20 U <sub>C</sub>   | 0,1 s     | 1,25 U <sub>MS</sub>  | 0,1 s    |
| Voltage decrease U<   | 0,80 U <sub>NS</sub>  | 1,5-2,4 s | 0,80 U <sub>NS</sub>  | 1,5-2,4s |
| Voltage increase U<<  | 0,45 U <sub>C</sub>   | 0,3 s     | 0,3 U <sub>MS</sub>   | 0,8 s    |
|                       | Connection to MV grid   |           | Connection to MV grid |          |
| Voltage increase U>>  | 1,15 U <sub>NS</sub>  | 0,1s      | 1,25 U <sub>NS</sub>  | 0,1 s    |
| Voltage decrease U<   | 0,80 U <sub>NS</sub>  | 1,0s      | 0,80 U <sub>NS</sub>  | 1,0 s    |
| Voltage decrease U << | 0,45 U <sub>NS</sub>  | 0,3 s     | 0,45 U <sub>NS</sub>  | 0,3 s    |

Important – Important – Important – Important – Important –  
Important

## Requirements for voltage relays (Ch. 10.3.1)

- Resetting ratio voltage increase  $\leq 1.02$
- Resetting ratio voltage drop  $\geq 0.98$
- Measurement error  $\leq 1\%$
- Analysis of fundamental oscillation root mean square

Ch. 10.3 Protection systems and protection settings (for power generating modules)

## Frequency Protection Systems

## Frequency protection systems

### BDEW 2008

- $\leq 47.5$  Hz      isolation from grid
- 47.5–51.5 Hz      isolation not permitted
- $\geq 51.5$  Hz      isolation from grid

### VDE-AR-N 4110

- $\leq 47.5$  Hz      isolation from grid
- 47.5–51.5 Hz      isolation not permitted
- 51.5-52.5 Hz      isolation permitted
- 52.5 Hz            isolation from grid

### PGU frequency protection systems

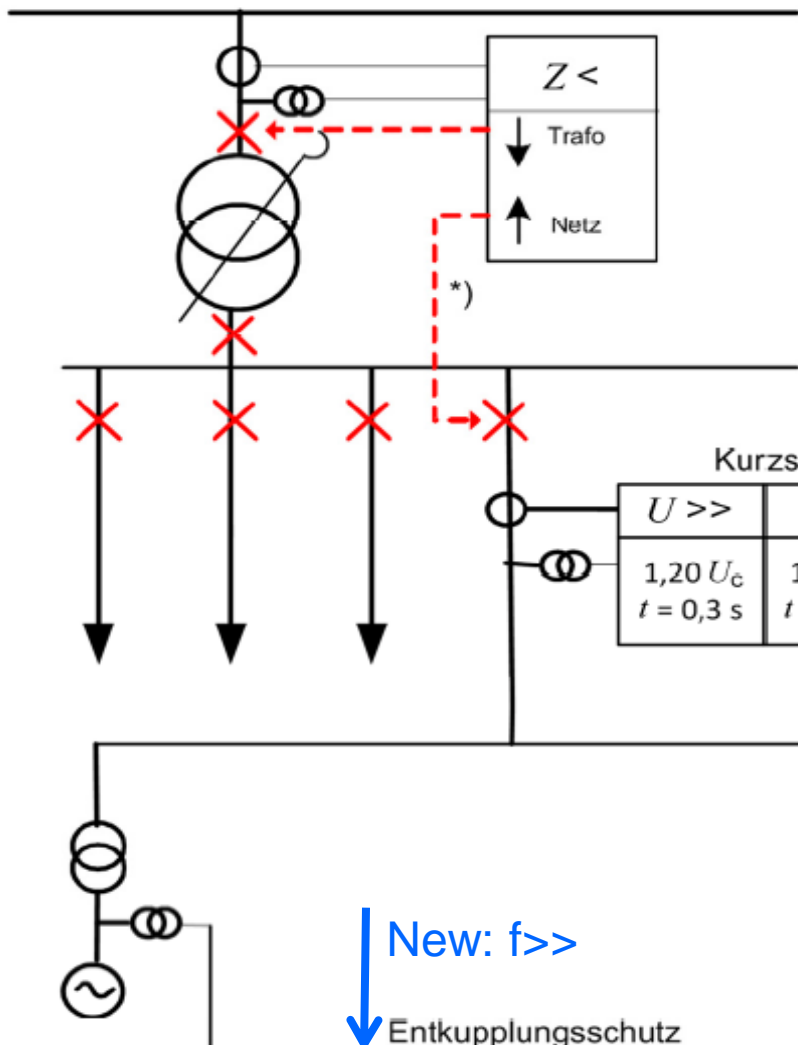
|                    |        |         |               |
|--------------------|--------|---------|---------------|
| Frequency decrease | $f <$  | 47.5 Hz | 0.1 s *       |
| Frequency increase | $f >$  | 51.5 Hz | $\leq 5$ s ** |
| Frequency increase | $f >>$ | 52.5 Hz | 0.1 s *       |

\* better: 5 repeat measurements

\*\* according to PGU property

## Ch. 10.3 Protection systems and protection settings (for power generating modules)

### **Protection overviews**



$U_c$ - vereinbarte Versorgungsspannung  
 $U_{NS} = U_c / \ddot{u}$  mit  $\ddot{u}$  = Übersetzungsverhältnis der Maschinentransformatoren

[ - - - ] Schutzfunktion ist konzeptionell zu berücksichtigen und nach NB-Vorgabe zu realisieren

\*) Mitnahmeschaltung nur bei im Stich angeschlossenen UW  
 \*\*) Auslösung LS am Netzanschlusspunkt nach 0,5 s

Kurzschlussschutz und übergeordneter Entkuppungsschutz

| $U \gg$                           | $U >$                             | $U <$                            | $f >$                            | $f <$                           | $Z <$   | $Q \rightarrow \& U <^{**}$       |
|-----------------------------------|-----------------------------------|----------------------------------|----------------------------------|---------------------------------|---|-----------------------------------|
| $1,20 U_c$<br>$t = 0,3 \text{ s}$ | $1,10 U_c$<br>$t = 180 \text{ s}$ | $0,8 U_c$<br>$t = 2,7 \text{ s}$ | 51,5 Hz<br>$t = 5400 \text{ ms}$ | 47,5 Hz<br>$t = 400 \text{ ms}$ | $U_F = 0,8 U_c$<br>$I_F = 0,2 I_N$<br>$I_E \geq 1,2 I_{CE}$ | $0,85 U_c$<br>$t = 0,5 \text{ s}$ |

$f >$  and  $f <$   
 optional (according to grid operator)  
 New: Distance relay with U/I-stimulus required  
 IOR not permitted

New:  $f >>$   
 Entkuppungsschutz

| $U \gg$                              | $U <$                                     | $U \ll$                             | $f \gg$                            | $f >$                        | $f <$                              |
|--------------------------------------|---|-------------------------------------|------------------------------------|------------------------------|------------------------------------|
| $1,25 U_{NS}$<br>$t = 0,1 \text{ s}$ | $0,8 U_{NS}$<br>$t = 1,5 - 2,4 \text{ s}$ | $0,3 U_{NS}$<br>$t = 0,8 \text{ s}$ | 52,5 Hz<br>$t \leq 100 \text{ ms}$ | 51,5 Hz<br>$t = 5 \text{ s}$ | 47,5 Hz<br>$t \leq 100 \text{ ms}$ |

New:  $f >>$   
 Entkuppungsschutz

| $U \gg$                              | $U <$                                     | $U \ll$                             | $f \gg$                            | $f >$                        | $f <$                              |
|--------------------------------------|---|-------------------------------------|------------------------------------|------------------------------|------------------------------------|
| $1,25 U_{NS}$<br>$t = 0,1 \text{ s}$ | $0,8 U_{NS}$<br>$t = 1,5 - 2,4 \text{ s}$ | $0,3 U_{NS}$<br>$t = 0,8 \text{ s}$ | 52,5 Hz<br>$t \leq 100 \text{ ms}$ | 51,5 Hz<br>$t = 5 \text{ s}$ | 47,5 Hz<br>$t \leq 100 \text{ ms}$ |

## Section 10.3

# Protection systems and protection settings - Frequency protection systems and protection overviews

